

1 **The performance analysis of a photo/thermal catalytic Trombe wall with energy**
2 **generation**

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10 **Abstract**

11 The Trombe wall (T-wall) has gained significant attention as an advanced building
12 envelope capable effectively harvest solar energy. Improving the functionality and
13 performance of the T-wall is critical for achieving energy-saving and positive energy
14 buildings. This study focuses on enhancing the functionality and performance of the T-
15 wall by incorporating with photovoltaic (PV) panels and aluminum panels in the T-wall
16 chamber. Additionally, the PV panels and aluminum panels are laminated with
17 photocatalyst and thermal materials to optimize their energy harvesting capabilities. In
18 this photo/thermal catalytic Trombe wall system, the air within the wall system moves
19 upwards due to thermal pressure and sweeps over the surface of the catalytic material
20 when exposed to solar irradiation. Through the combined effects of solar energy and
21 catalytic oxidation, the cold and dirty air in the chamber undergoes heating and
22 purification processes, resulting in the desired heating effect while significantly
23 improving the overall air quality within the environment. The experimental results
24 highlight that the novel T-wall system offers a multifunctional solution that addresses
25 electricity generation, heating, and improvement of indoor air quality. The main
26 findings of this study are as follows: (1) During the period from 9:00 to 16:00, the T-
27 wall system demonstrates the ability to provide a range of 6.25 kJ/mol to 17.74 kJ/mol

28 of heat and 0.075 kWh to 0.372 kWh of electricity per day. (2) In terms of indoor air
29 quality improvement, the T-wall system exhibits a one-way sterilization efficiency of
30 bacterial aerosols ranging from 0.204 to 0.347. (3) The comprehensive performance of
31 the system was found to be optimal when the system spacing is 25 cm. (4) In terms of
32 the layout of UV light, it was observed that at the top and bottom of the system yielded
33 better sterilization efficiency.

34 **Keywords:** T-wall; sterilization; the severe cold region; catalytic oxidation; energy
35 production.

36 **1. Introduction**

37 With the rapid development of society, there has been a growing focus and concern
38 about building energy consumption in recent years [1-3]. Currently, buildings account
39 for a substantial 40% of total global energy consumption [4]. The energy consumption
40 for heating, ventilation, and air conditioning (HVAC) represents more than 50% of the
41 total energy consumption of buildings [5]. As a clean energy source, solar energy has
42 the potential to reduce fossil energy consumption and carbon emissions in buildings. T-
43 Wall, as an advanced building envelope that can effectively harvest solar energy, is
44 gaining increasing attention. The T-wall utilizes solar radiation to facilitate airflow
45 within the chamber, making use of the innovated feature not only minimize the energy
46 needed for room heating but also enhance air circulation and improve indoor air quality
47 [6-8]. The T-wall offers an exceptional solution for achieving remarkable ventilation
48 performance. By utilizing solar energy to drive airflow and empower natural ventilation,
49 it efficiently combines ventilation technology with advanced building envelope
50 technology [9].

51 Several researchers have focused on optimizing the construction of the T-wall to
52 improve its performance [10-12]. Ji et al. [13] incorporating PV cells onto the glazing
53 cover of a conventional T-wall. The experimental findings demonstrated that this
54 innovative approach achieved average electrical efficiency of 10–11%. Moreover, the

55 room equipped with the novel T-wall experienced a maximum temperature increase
56 of 14.42°C. Kong et al. [14] proposed a novel design that is double-layer phase change
57 T-wall with multiple phase change. Though optimization, this design resulted in a
58 significant increase in indoor temperature during winter, ranging from 0.3 to 6.6°C.
59 Furthermore, it achieved a notable reduction in heat flux by 1.8% to 75.7%. Zhang et
60 al. [15] proposed a novel T-wall with heat pipes, which efficiently reduce heat loss by
61 an average of 56%, the cumulative heat loss was decreased by 5.29 kWh/m². Building
62 upon this concept, Zhang et al. [16-18] further combined the thermoelectric module and
63 a PV module with T-wall, creating a hybrid wall system. This innovated hybrid wall
64 system offered multiple functionalities, including year-round electricity, space heating
65 in heating seasons, and cooling in cooling climate. Zhu et al. [19] and Duan et al. [20]
66 explored the combination of phase change materials (PCM) with the T-wall. They
67 focused on determining the optimal phase change temperature and investigated the
68 suitable PCM range for integration with the T-Wall. He et al. [21] introduced a Venetian
69 solar collector wall by incorporating a louver within the air gap to selectively cover the
70 absorbent cover. The new type of T-wall can improve room temperature and thermal
71 environment while minimizing the space heat load to a significant extent.

72 To further expand the capabilities of the T-wall, researchers have begun exploring the
73 integration of indoor air quality (IAQ) control technology with the T-wall. Given the
74 heightened emphasis on creating a healthy living environment, particularly in light of
75 the COVID-19 pandemic, enhancing IAQ has become an essential and unavoidable
76 requirement [22-24]. Bioaerosols transmission, as one of the indoor air pollutants, poses
77 a significant threat to public health, especially in enclosed indoor environments [25-27].
78 In the severe cold region of China, characterized by long, cold winters, people tend to
79 avoid opening windows for ventilation to maintain room warmth. Consequently,
80 Chinese energy efficiency standards [28,29] impose stringent requirements on building
81 airtightness in these region. This leads to limited exchange of indoor air with the outside
82 environment, resulting the accumulation of pollutants within the building. As a result,

83 individuals face an high risk of infection due to the heightened concentration of
84 pollutants in enclosed spaces [30-32]. Photocatalysis is considered as a new sterilization
85 method in disinfection of pathogenic bacteria [33]. It not only exhibits a strong
86 sterilization effect but also effectively decomposes the endotoxin produced by bacteria
87 with low side effects. This characteristic demonstrates its great potential for bactericidal
88 and antibacterial activities [34-36]. This findings have important implications for the
89 control of respiratory infectious diseases within buildings [37]. He et al. [38] and Yu et
90 al. [39] have conducted research on combining photocatalytic oxidation with T-wall. In
91 their study, they utilized the UV light in solar radiation to initiate photocatalytic
92 purification reaction. Yu et al. [40] combined the photocatalytic technology with a T-
93 wall, enabling simultaneous space heating and indoor air purification. This system
94 achieved impressive results, with a daily air heating efficiency of 41.3% and a total
95 generated volume of fresh air reaching $249.2 \text{ m}^3/(\text{m}^2 \cdot \text{day})$.

96 Additionally, thermal catalytic is also a commonly used sterilization method. It is
97 often more efficient than photocatalysis due to its high energy consumption. Thermal
98 catalytic offers several advantages, including high removal efficiency, simple
99 equipment, and the absence of secondary pollution [41]. Under solar irradiation, the air
100 temperature within the T-wall chamber can reach a range of 60–100°C [42]. It is
101 important to note that a temperature of 45°C has the ability to inhibit the self-repair
102 mechanisms of bacteria's DNA and RNA of bacteria, while the temperature above 55 °C
103 can efficiently destroy bacterial DNA and RNA [43]. Yu et al. [44] propose a novel T-
104 wall based on thermal sterilization. The T-wall demonstrates an average daily air
105 thermal efficiency of 0.46, showcasing excellent energy-saving and purification
106 performances in the heating season. A series of experiments [45] and numerical studies
107 [46] have also been conducted to further investigate its performance.

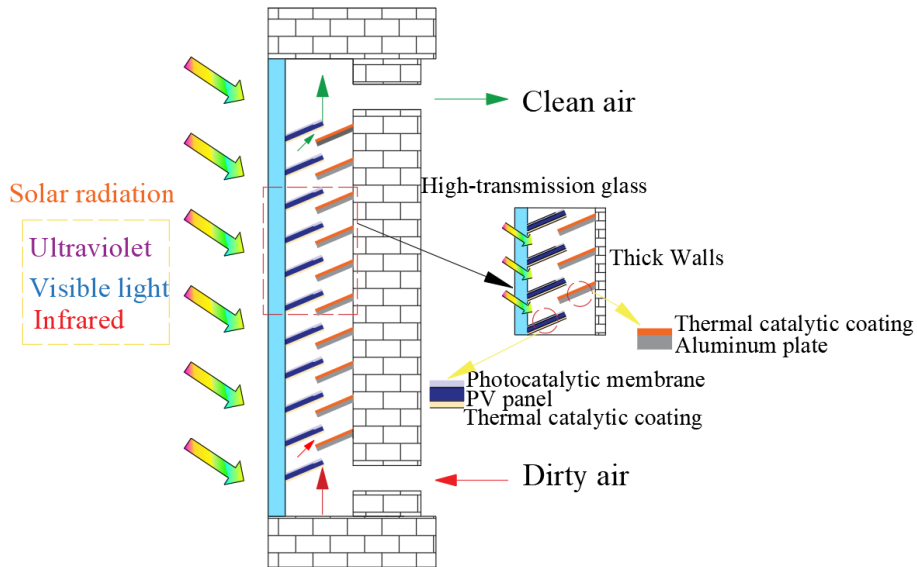
108 Currently, the newly proposed T-wall faces certain challenges, including low system
109 efficiency and incomplete functionality. It is worth noting that the reported papers
110 primarily concentrate on thermal efficiency and inorganic purification efficiency of

111 the novel T-wall. Only a limited number of studies have explored the potential of the
112 novel T-wall for electricity generation, heating, and sterilization. The optimum spacing
113 of the T-wall and the optimum position of the system's UV light strips have not been
114 clearly determined yet. in light of these challenges, it is both meaningful and necessary
115 to optimize the structural parameters of the T-wall and enhance its functionality. To
116 accomplish this objective, the present study was carried out to propose an advanced
117 envelope based on the T-wall. The novel T-wall chamber has an increased flow path
118 and a larger contact area between the pollutants and the catalytic material, which
119 improves the purification efficiency. Additionally, the integration of PV panels within
120 the chamber allow for generation of electrical power. The air flowing inside the
121 chamber due to the thermal pressure carries away the heat from the PV panels and
122 increases the efficiency of electricity generation [47]. In this work, the main works
123 included that: (1) a novel T-wall was proposed, and conducted the performance analysis
124 of heating, electricity generation, and sterilization efficiency (2) the structural
125 parameter of the novel T-wall was optimized. (3) The sterilization efficiency of the
126 system was further enhanced by the arrangement of UV light strips in the chamber of
127 the T-wall. The placement of the UV light strips in the chamber was investigated. With
128 this study, a multi-functional wall that integrates building envelope with solar energy
129 systems becomes a viable possibility. This advancement serves as a valuable reference
130 for the implementation of energy-saving practices, the realization of positive energy
131 buildings, and the effective control of the indoor environment. By combining various
132 functionalities into a single system, this research contributes to the pursuit of
133 sustainable and efficient building designs.

134 **2. System description**

135 **Fig. 1** shows the schematic diagram of the novel T-wall. The components of the novel
136 T-wall consist of high-transmission glass, PV panels with photocatalytic and thermal
137 catalytic coatings, aluminum panels with thermal catalytic coatings, a chamber, thick

138 walls, and an air inlet and air outlet. The high transmission glass and the thick walls
139 form the T-wall chamber which is connected to the indoor environment. Air inlet and
140 air outlet are set at the top and bottom of the thick walls to allow air to circulate between
141 the chamber and the room.



142

143 **Fig. 1.** The schematic diagram of the novel T-wall

144 In the T-wall chamber, cold air from the room enters through the lower air inlet. As the
145 solar irradiation heats the air within the chamber, it creates thermal pressure, causing
146 the air to flow upwards. To enhance the performance of the chamber, the PV panels
147 have been integrated with aluminum panels in a baffle-like configuration. This design
148 increases the distance traveled by the airflow within the chamber, allowing for a more
149 extensive contact between the pollutants and the catalytic material.

150 Following the airflow and heating process, the catalytic reaction takes place within the
151 T-wall chamber, causing the pollutants to be decomposed. As a result, the clean air
152 leaves the chamber through the upper air outlet, establishing a circulation with the
153 indoor air and heating the room at the same time.

154 When sunlight reaches the PV and aluminum panels, the ultraviolet part of the solar
155 radiation undergoes a photocatalytic reaction on the TiO_2 membrane present on the
156 surface of the PV panels. Simultaneously, the visible part of the solar radiation that
157 reaches the PV panels is converted into electricity, which can be utilized to power

158 various indoor appliances and systems or stored for later use. The remaining infrared
159 part of the solar radiation is converted into thermal energy, which raises the temperature
160 of the PV and aluminum panels. In addition to the aforementioned processes, the
161 thermal catalytic material applied to the PV and aluminum panels exhibits a high a high
162 absorption rate of solar radiation in the infrared part. Driven by the high temperature, a
163 thermal catalytic reaction takes place when the catalytic temperature is approached.
164 This reaction effectively degrades the airborne pollutants present in the T-Wall system.
165 With the integration of these mechanisms, the novel T-wall design enables a
166 comprehensive and efficient utilization of sunlight, ensuring optimal energy utilization
167 and air purification capabilities.

168

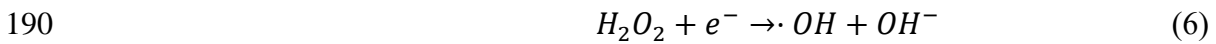
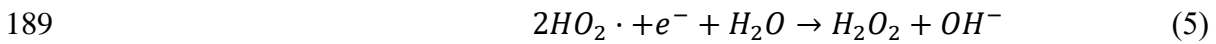
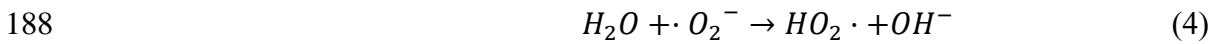
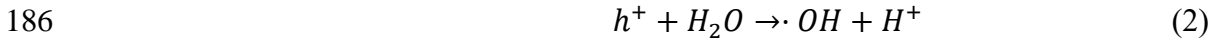
169 **3. Experiment**

170 The experiment was conducted during the period of October to November 2022, with
171 a duration of 9:00 - 16:00. The experiment setup was situated on the roof of a school
172 located in Harbin, Heilongjiang Province, China. To simulate the presence of airborne
173 pollutants, a certain concentration of *Serratia marcescens* suspension was prepared and
174 uniformly sprayed into the environmental chamber using an aerosol generator. The
175 environmental parameters of the environmental chamber have been set to simulate an
176 indoor environment of 22°C and 60% relative humidity. The bacterial aerosol is mixed
177 in the environmental chamber and then enters the novel T-wall under thermal pressure.
178 The air inlet and air outlet were closed during the night time.

179 **3.1 Photo and thermal catalytic material**

180 In this study, a TiO₂ membrane was employed as the photocatalytic material on the
181 surface of the PV panels. TiO₂ will produce strong oxidizing substances under
182 ultraviolet light. Among them, ·O₂⁻ and ·OH has strong oxidation. As shown in **Eq. (1)**

183 to **Eq. (7)** Strong oxidizing substances will destroy the permeability of the bacterial
 184 membrane and DNA / RNA structure to achieve the effect of sterilization.



192

193 Due to the half-wave loss of reflected light in the film, some optimization of the
 194 membrane thickness is required. As shown in **Eq. (8)**:

195
$$D = \frac{(2k+1)\lambda_0}{4} (k = 1, 2, 3 \dots \dots) \quad (8)$$

196 D is the calculated film layer thickness, $\lambda_0 = 550$ nm. According to the theory of
 197 optical membrane layer design, when the membrane layer thickness d conforms to **Eq.**
 198 **(8)**, it can weaken the intensity of reflected light and increase the intensity of transmitted
 199 light, which plays a role in increasing the transmission. In this experiment, the thickness
 200 of the photocatalytic membrane is 62 μ m, which satisfies the condition of the increased
 201 transmission film.

202 **Fig. 2** shows the I-V curves for the PV panels. Without the membrane, the peak power
 203 is 0.055 w. However, with the inclusion of membrane, the peak power output decreased
 204 slightly to 0.051 w, representing approximately 92.7% the power output achieved
 205 without the membrane. Hence, it can be concluded that the addition of the
 206 photocatalytic membrane has not much effect on the power generation efficiency of the
 207 PV panel.

(a)

(b)

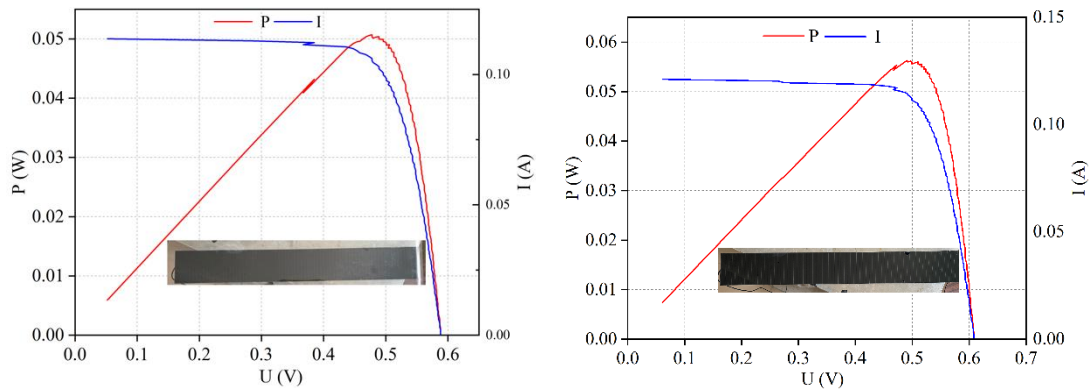


Fig. 2. Photograph of the PV panels (a) with film and (b) without film

208

209 In this experiment, $\text{MnO}_x - \text{CeO}_2$ was used as the thermal catalytic material. $\text{MnO}_x -$
 210 CeO_2 absorbs the infrared and visible wavelengths of sunlight and serves two purposes
 211 in the T-Wall system. Firstly, it helps in indoor heating by capturing solar energy.
 212 Secondly, it facilitates thermal, aiding in the degradation of pollutants. When combined
 213 with bacteria, $\text{MnO}_x - \text{CeO}_2$ can effectively destroy the bacterial cell membranes
 214 through infrared-triggered heat therapy, converting infrared radiation into heat and
 215 achieving photothermal conversion, using high temperatures to purify microorganisms.
 216 $\text{MnO}_x - \text{CeO}_2$ can also release metal particles that will pass through the cell membrane
 217 and destroy cell components after contacting bacterial cells [33,48].

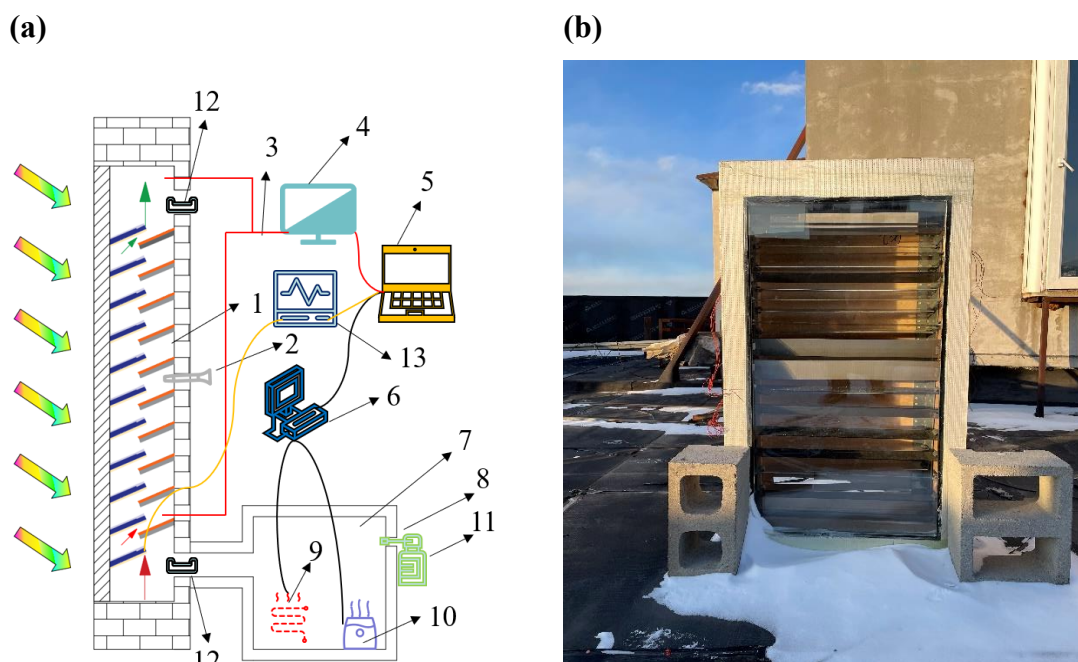
218 However, the application of thermal catalytic is limited because its catalytic effect is
 219 unstable, and its sterilization performance is not as good as photocatalysis. Therefore,
 220 in this study, thermal catalysis was only used as a secondary means of indoor air
 221 purification and the main means of purification is photocatalysis.

222

223 3.2 Experimental set-up

224 In order to study the heat production, electricity production, and bacterial sterilization
 225 performance of the novel T-wall, an experimental test system was set up. **Fig. 3** shows
 226 the schematic diagram and photos of the experimental setup of the novel T-wall.
 227 Thermocouples were arranged at the air inlet and outlet of the novel T-wall to monitor
 228 temperature, and Petri dishes were arranged to sample bioaerosol concentrations. The

229 temperature data were recorded using a paperless recorder and transferred to the
 230 computer. In the environmental chamber, electric heaters and ultrasonic humidifiers
 231 were arranged to simulate the room air parameters. The parameter values set for the
 232 environmental chamber were 22°C and 60% RH. Proportion integration differentiation
 233 (PID) is used to control the ambient parameters in the environmental chamber to
 234 maintain the set values. A hot-wire anemometer was also arranged in the middle of the
 235 T-wall to test the airflow speed inside the T-wall. The dimensions of the experimental
 236 set-up are presented in **Table 1**.
 237



238 **Fig. 3.** The (a) schematic diagram and (b) photograph of the experimental set-up. (1)
 239 The novel T-wall. (2) Hot-wire anemometer. (3) Thermocouple. (4) Data acquisition
 240 instrument. (5) Computer. (6) Proportion integration differentiation controller. (7)
 241 Environmental chamber. (8) Pressure hole. (9) Electric heater. (10) Ultrasonic
 242 Humidifier. (11) Aerosol generator. (12) Petri dish. (13) IV-curve tester.

243

244 **Table 1.** The dimensions of the experimental set-up.

Components	Values (Length × Width × Height)
------------	----------------------------------

T-wall	0.6 m × 0.3 m × 1.2 m
Environmental chamber	0.6 m × 0.6 m × 0.6 m
Pressure hole	0.02 m × 0.02 m (Ignore Width)
Air inlet or Air outlet	0.15 m × 0.6 m (Ignore Width)

245

246 The PV panels used in this study were purchased from Advanced Solar Power
 247 (Hangzhou) Inc. The specification parameters of the used PV panels under standard
 248 testing conditions (solar radiation: 1000 W/m², testing temperature: 25°C) are listed in
 249 **Table 2.**

250 **Table 2.** The specification parameters of per PV panel.

Parameters	Values
Model	ASP 600x80-73
Length	600 mm
Width	150 mm
Thickness	3.2 mm
Maximum Power (P _{max})	5.2 W
Voltage at Maximum Power (V _{mp})	42.0 V
Current at Maximum Power (I _{mp})	0.123 A
Temperature coefficient of maximum power	-0.214%/°C

251

252 Experimental test parameters include temperature, airflow velocity, electrical
 253 parameters, solar radiation intensity, and bacterial aerosol concentration. Electrical
 254 parameters were recorded every 1 minute using the IV-curve, to which the PV panels
 255 were connected. A hot-wire anemometer measured the wind speed in the middle of the
 256 chamber. Thermocouples recorded the inlet and outlet air temperatures of the novel T-
 257 wall. The thermocouple was connected to the data collector, and the data was recorded
 258 every 10 seconds. The experimental accuracies of the measuring instruments are shown
 259 in **Table 3.**

260

261 **Table 3.** The accuracies of the main experimental measuring apparatus.

Apparatus	Model	Measuring parameter	Accuracy
Hot-wire anemometer	KANOMAX	Airflow velocity	± 0.01 m/s
IV-curve	PROVA – 200A	Electricity generation	1% of V ± 0.09 V, 1% of I ± 9 mA
Thermocouple	TT–T-30	Temperature	$\pm 0.5^{\circ}$ C

262

263 In this experiment, *Serratia marcescens* was used as the bioaerosol. The safety level of
 264 *Serratia marcescens* is BSL-1(biological safety level of 1). This kind of bacterium can
 265 produce red dendritic colonies after 24-36 h incubation at 20-35°C, which is not
 266 harmful to the individuals involved in the experiment, and its particle size and density
 267 are representative. The method of bioaerosol sampling has been mentioned in the
 268 previous study, using Luria-Bertani agar for bioaerosol sampling.

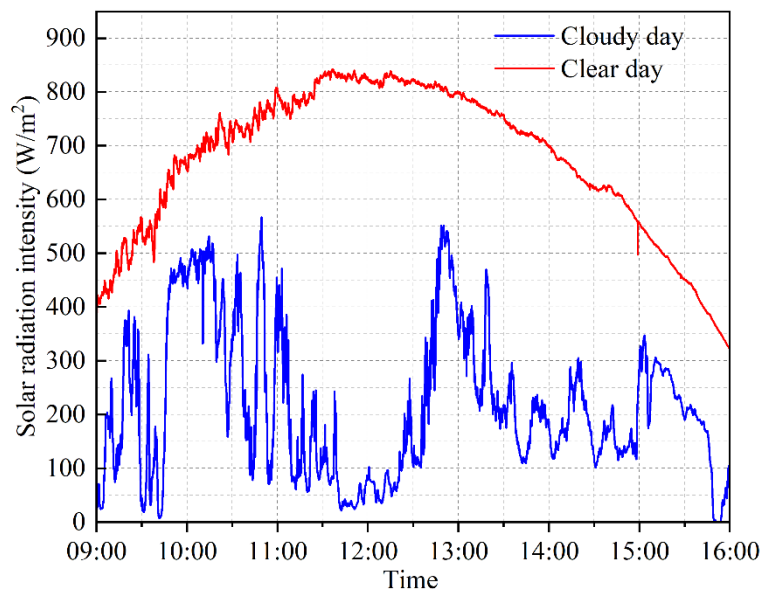
269 The heat production and power generation potential of the novel T-wall was
 270 investigated in the severe cold region of China (**Section 4.1**), the structural parameters
 271 of the new T-wall were optimized, and the optimal spacing between chambers was
 272 analyzed (**Section 4.2**). The degradation efficiency of different concentrations of
 273 *Serratia marcescens*, at different moments, was also tested (**Section 4.3**). Finally, the
 274 effect of the layout of the UV light strips based on the self-generated power of the new
 275 T-wall was analyzed (**Section 4.4**).

276

277 **4. Results and discussions**

278 **4.1 The performance of heating, electricity generation, and**
279 **sterilization efficiency**

280 The meteorological data in Harbin was tested. **Fig. 4.** shows the tested solar radiation
281 intensity on sunny and cloudy days in Harbin, spanning from October 27th to
282 November 20th. The subsequent investigation and comparison for the T-wall systems
283 were conducted based on the performance calculations on sunny and cloudy days. The
284 average solar radiation intensity of sunny and cloudy days is 527.6 W/m^2 and 272.2
285 W/m^2 , respectively. The indoor temperature and relative humidity were set at 22°C and
286 60% , respectively. During the experiment, the indoor upper and lower ventilation
287 baffles were kept in an open status from 9:00 to 16:00. To maintain the desired indoor
288 conditions, electric heaters or ultrasonic humidifiers were activated when the air
289 temperature and relative humidity in the airflow channel fell below the setting air
290 temperature and relative humidity.



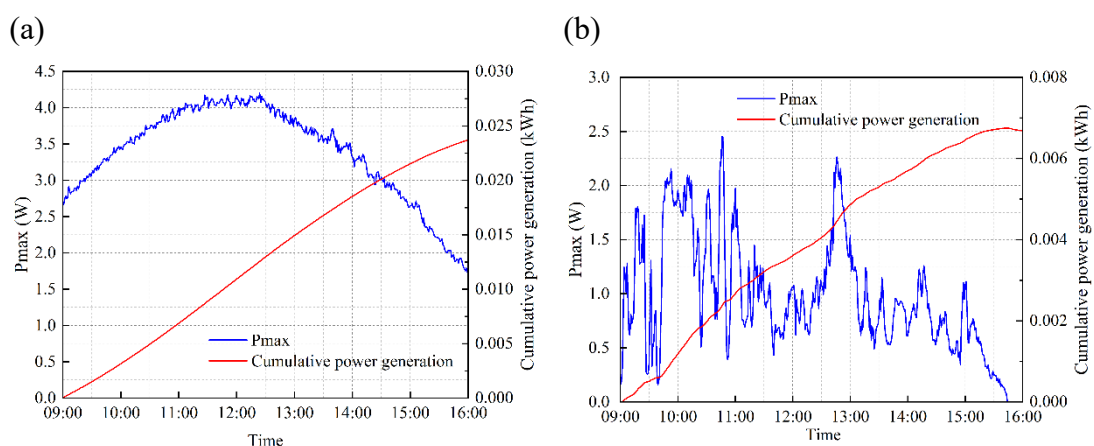
291

292 **Fig. 4.** The tested solar radiation intensity on sunny and cloudy days in Harbin

293

294 **Fig. 5.** shows the electricity generation per PV panel on cloudy and sunny days. During

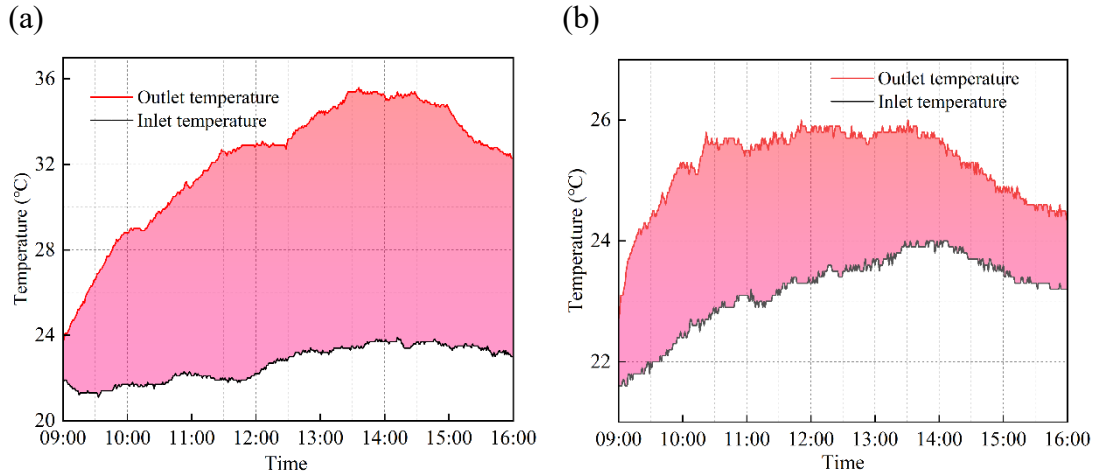
295 the test period, the average power of the T-wall system is 3.41 W on sunny days and
 296 0.62 W on cloudy days. The average power presents a similar variation trend with the
 297 solar radiation intensity. On sunny days, the power generated by the T-wall system
 298 approached its maximum of 4.14 W at 12:15 p.m. However, on cloudy days, the
 299 power generation did not exhibit a clear pattern or regulation. The cumulative power
 300 generation for a full day was recorded as 0.0248 kWh on sunny days and 0.005 kWh
 301 on cloud days. Considering that the T-wall system consists of 12 identically arranged
 302 PV panels, the cumulative power generation for a full day can range from 0.06 kWh to
 303 0.298 kWh. It can be seen that meteorological data has a great effect on the power
 304 generation of the novel T-wall system. The power generation on sunny days is
 305 approximately 4.96 times higher compared to that on cloudy days.



306 **Fig. 5.** The electricity generation of the system on (a) sunny days and (b) cloudy days
 307

308 **Fig. 6.** shows the plots of the air inlet temperature, air outlet temperature and
 309 temperature difference between air inlet and air outlet, respectively. On sunny days, the
 310 air outlet temperature ranges from 23.7 to 35.6°C when the air inlet temperature ranges
 311 from 21.1 to 23.9°C. Similarly, on cloudy days, the air outlet temperature ranges from
 312 22.7 to 26°C when the air inlet temperature ranges from 21.6 to 23.7°C. The
 313 temperature difference between air inlet and air outlet is 9.6°C and 3.9°C on sunny and
 314 cloudy days, respectively. On sunny days, the temperature difference between air inlet
 315 and air outlet of the T-wall system exceeds 10°C for approximately 57% of the total
 316 experimental time. The air outlet temperature is posteriority compared to the solar

317 radiation intensity on sunny days. The air outlet temperature approached the maximum
 318 temperature at 13:40 p.m. Although the maximum temperature was obtained at 13:40
 319 p.m., the air outlet temperature usually ascended until 14:29 p.m. Unlike sunny days,
 320 there is no clear pattern or regulation observed for the air outlet temperature on cloudy
 321 days. The air outlet temperature on cloudy days rises to 25.7°C at 10:27 a.m. and
 322 remains relatively stable at this value. It starts to decline after 13:32 p.m.



323 **Fig. 6.** The plots of the air inlet temperature, air outlet temperature on (a) sunny days
 324 and (b) cloudy days
 325

326 **Fig. 7.** shows the solar heat gain of the T-wall system. According to the measurement
 327 results of the hot-wire anemometer, the airflow in the range of 0.01–0.096 m/s. The
 328 instantaneous heat gain can be calculated by the heat quantity formula, shown as **Eq.**
 329 **(9)**:

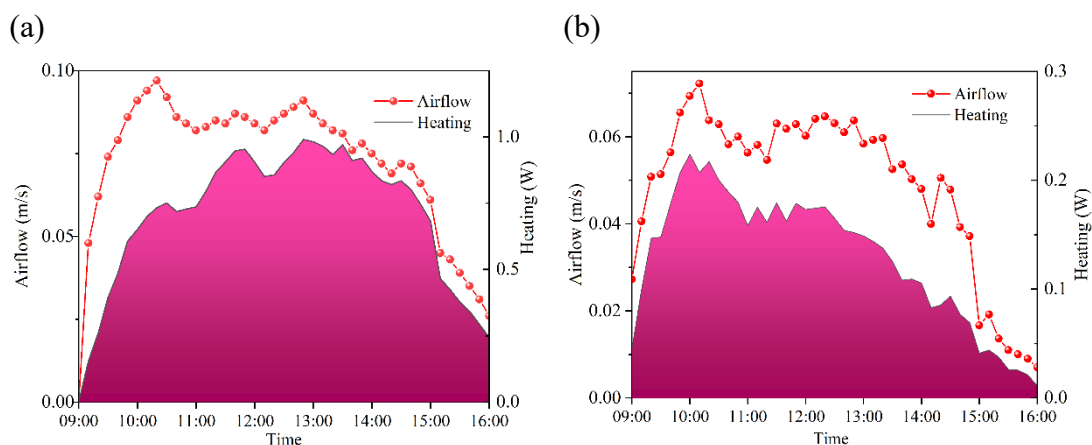
$$Q_{heat} = C_{Air}AV(T_{out} - T_{in}) \quad (9)$$

331 Where V , m/s is the airflow in the T-wall chamber and C_{Air} , J/(kg K) is the specific
 332 heat of air. T_{out} and T_{in} are air inlet temperature and air outlet temperature,
 333 respectively. A , m² is the area of the air outlet. The daily thermal efficiency, which is
 334 shown in **Eq. (10)**, can be obtained from the time integral of **Eq. (9)**:

$$\overline{Q_{heat}} = \int C_{Air}AV(T_{out} - T_{in})dt \quad (10)$$

336 The T-wall system can provide 17.74 kJ/mol heat on sunny days and 6.25 kJ/mol on
 337 cloudy days. The heat gain in the T-wall chamber is not solely determined by the solar

338 radiation intensity. It is also influenced by the airflow within the T-wall chamber. The
339 airflow plays a significant role in determining the heat gain, in addition to the
340 temperature difference resulting from solar radiation intensity. From **Fig. 7**, it is evident
341 that on sunny days, the heat gain remains consistently high from 11:49 a.m. to 14:36
342 a.m. Interestingly, the heat gain does not peak when the airflow reaches its maximum.
343 This can be attributed to the fact that the temperature difference between the air inlet
344 and air outlet is not at its maximum during that period (as shown in **Fig. 6**), resulting in
345 a smaller heat gain. On cloudy days, The heat gain days reaches its maximum at 10:02
346 a.m. and subsequently decreases, following a similar trend as the airflow.



347 **Fig. 7.** The heat gain of the T-wall system on (a) sunny days and (b) cloudy days

348

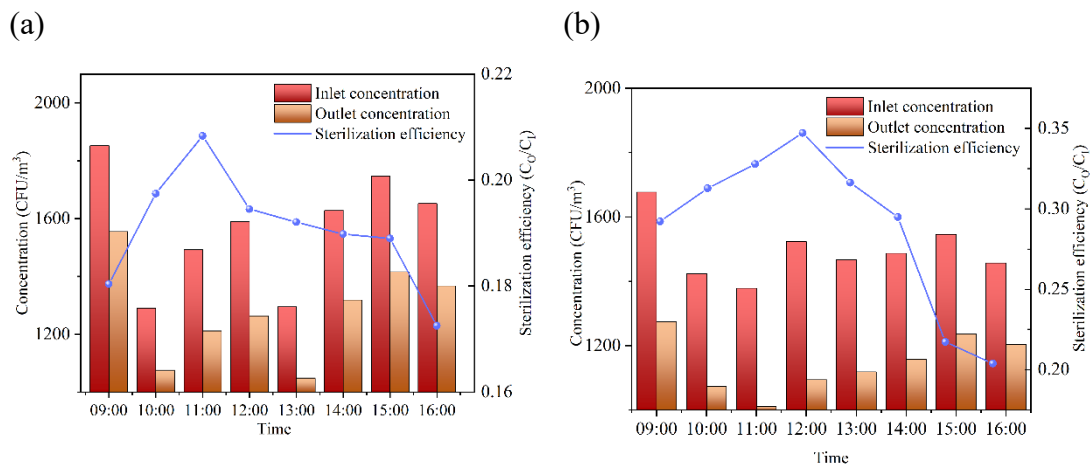
349 To investigate the sterilization efficiency of the different bacterial aerosol
350 concentrations, the sterilization efficiency of *Serratia marcescens* bioaerosols under
351 experimental and control groups was measured. The control group has a similar
352 structure to the experimental group, but it does not contain any catalytic material. The
353 PV and aluminum panels in the experimental group were coated with photocatalytic
354 membranes and thermal catalytic materials. The same dose of *Serratia marcescens*
355 bacterial aerosol was sprayed at each hour to measure the change in sterilization
356 efficiency over time. In this study, the concentration of sprayed bacterial aerosols was
357 1500 ± 100 CFU/m³. All sterilization efficiency in this study refers to one-way
358 sterilization efficiency. The sterilization efficiency of bacterial aerosols is expressed as

359 follows:

360
$$\eta_{sterilization}(\%) = \left(1 - \frac{CFU_{outlet}}{CFU_{inlet}}\right) \times 100\% \quad (11)$$

361 Where CFU_{outlet} and CFU_{inlet} are the concentration of bacterial aerosols at the
362 outlet and inlet.

363 **Fig. 8** shows the sterilization efficiency versus time of experimental and control groups.
364 The sterilization efficiency of control group and experimental group were in the range
365 of 0.172-0.208 and 0.204-0.347 calculated by **Eq.(11)**, respectively. This shows that
366 catalytic oxidization can effectively enhance the indoor air purification effect. The slow
367 change in the sterilization efficiency curve over time for the control group indicates that
368 the absence of catalytic oxidation in the control system limits its ability to effectively
369 sterilize the air. In the control group, sterilization efficiency primarily relies on
370 sedimentation. The sterilization efficiency of the experimental group was influenced by
371 solar radiation. Sterilization efficiency reaches a maximum value of 0.347 at noon when
372 solar radiation was at its peak. However, as solar radiation decreased throughout the
373 day, the efficiency of sterilization gradually decreased as well. By the time of sunset,
374 the sterilization efficiency of both the control and experimental groups had become
375 equal.



376 **Fig. 8.** The sterilization efficiency of (a) control group and (b) experimental group

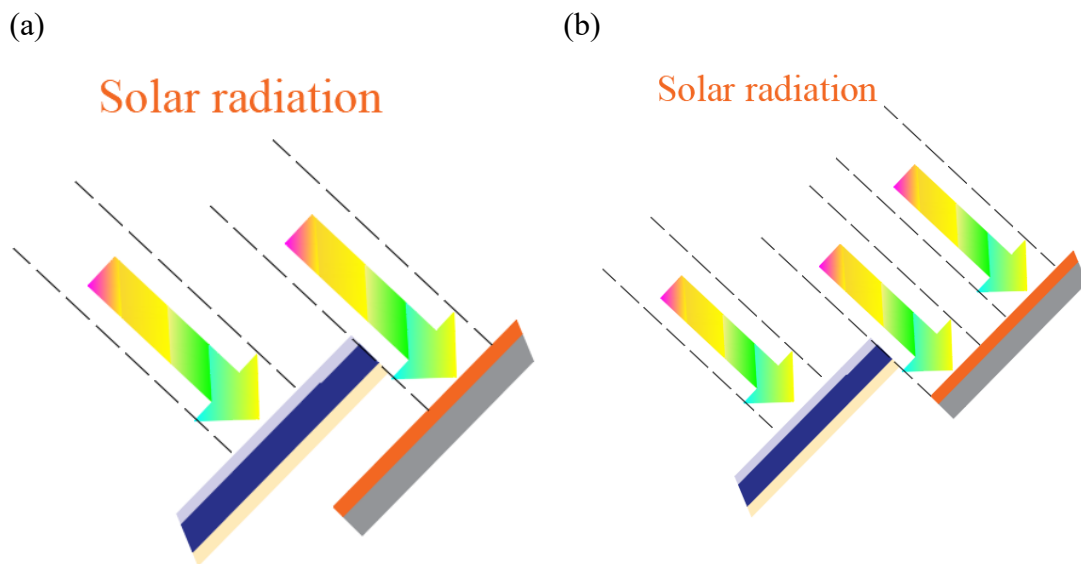
377

378 The integration of catalytic oxidation and T-wall has led to a significant improvement

379 in sterilization efficiency. The system achieved a one-way sterilization efficiency
380 ranged from 0.204 to 0.347 for bacterial aerosols, indicating promising application
381 prospects for solar-powered indoor air purification. After long-term cyclic inactivation,
382 the indoor bacterial aerosol concentration will descend to a harmless level.
383

384 4.2 Optimal spacing of the T-wall system

385 In this part, the performance of heating, electricity generation, and sterilization
386 efficiency under different chamber spacing have been calculated. The chamber spacing
387 is ranged from 35 cm to 15 cm, with an interval of 5 cm. The schematic diagram of the
388 T-wall system spacing is shown in **Fig. 9**. It can be seen that the spacing has an
389 important effect on the T-wall electricity generation performance. When the spacing is
390 small, the baffles tend to block each other, resulting in reduced exposure to solar
391 radiation.

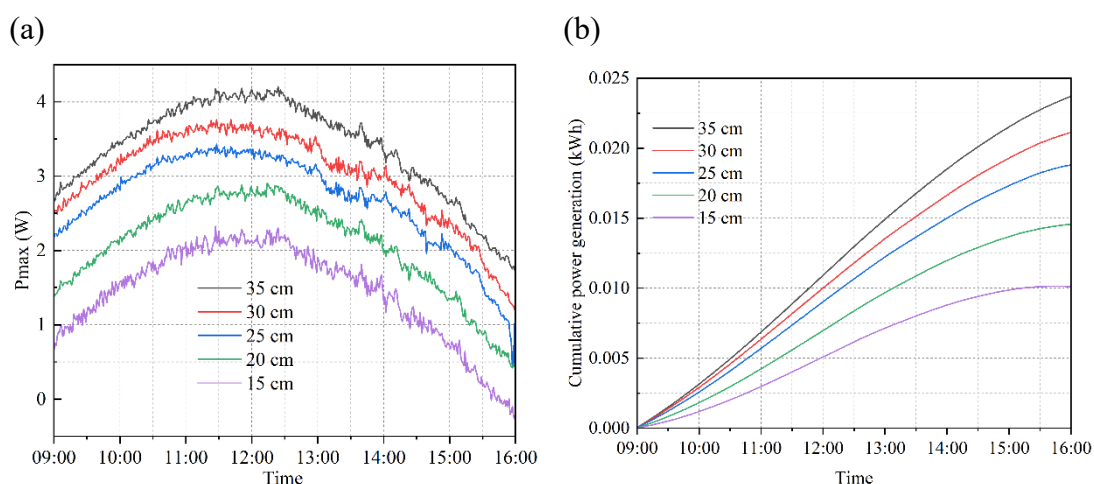


392 **Fig. 9.** Schematic diagram of T-wall system spacing. (a) small spacing and (b) large
393 spacing

394

395 **Fig. 10** shows the electricity generation of the T-wall system under different spacing.
396 The electricity generation of the system continuously reduced as the spacing between

397 the baffles decreased. The electricity generation of the system shows a similar trend
 398 across different spacing values. The average power observed for different spacing
 399 configurations, ranging from 35 cm, 30cm, 25cm, 20 cm to 15 cm, were 3.4 W, 3.0 W,
 400 2.6 W, 2.1 W, and 1.4 W, respectively. This trend demonstrates that the spacing has an
 401 increasingly significant impact on the electricity generated as it decreases. Because
 402 when the spacing is reduced by 5 cm, the average electricity generation shows an
 403 increase from 0.4 W to 0.5 W, and finally reaches 0.7 W. When the spacing decreases
 404 from 35 cm to 15 cm, the cumulative electricity production per PV panel is 0.0248
 405 kWh, 0.0211 kWh, 0.0188 kWh, 0.0146 kWh, and 0.0101 kWh, respectively. Similar
 406 to the average power, the cumulative electricity generation does not reduce equally as
 407 the spacing decreases. An inflection point occurs at 25cm, where the reduction in
 408 system electricity generation increases for every 5cm reduction in spacing.



409 **Fig. 10.** The electricity generation of the T-wall system under different spacing. (a)
 410 power and (b) cumulative power generation

411

412 For bacterial aerosol concentration, it is mainly affected by sedimentation and catalytic
 413 oxidation. The impact of sedimentation has been analyzed in the control group in
 414 **Section 4.1.** The reaction rate of photocatalysis is shown in **Eq. (12):**

415
$$r = -\frac{dC_s}{dt} = \frac{k_r K C_s}{(1 + K C_s)} \quad (12)$$

416 Where r , mg/(L*min), is the reaction rate. C_s , mg/L, is the pollutant concentration. t ,

417 min, is the reaction time. k_r , min^{-1} , is the reaction rate constant. K is the adsorption
418 constant. k_r and K is determined by many factors in the reaction, including light
419 intensity, initial concentration of pollutants, reaction temperature, physical properties
420 of reactants, oxygen concentration, etc.

421 **Fig. 11** shows the sterilization efficiency of the T-wall system under different spacing.
422 The sterilization efficiency increased as the spacing decreased . Similar to the **Section**
423 **4.1**, sterilization efficiency reaches its maximum value at noon. The average
424 sterilization efficiency for spacing values of 35 cm, 30 cm, 25 cm, 20 cm, and 15 cm
425 are 0.365, 0.356, 0.343, 0.267, and 0.202, respectively. The highest sterilization
426 efficiency of 0.448 can reached when the spacing is 15cm. When the spacing is
427 decreased to 25cm, further decreasing the spacing has minimal impact on improving
428 bacterial sterilization efficiency. This can be explained as the adsorption of bacterial
429 aerosols on catalyst surfaces. As can be seen from **Eq. (12)**, reaction time has an effect
430 on catalytic sterilization. The reaction rate of the bacterial aerosol decreases as the
431 reaction time with the catalyst increases. As the spacing decreases, the volumetric flow
432 rate of the bacterial aerosol increases, which can affect the catalytic oxidation reaction.
433 The volumetric flow rate effect is ultimately manifested by the adsorption of pollutant
434 gas molecules on the catalyst surface. Once the spacing is decreased to 25cm, the
435 volumetric flow rate has approached its maximum value. Further reduction of the
436 spacing has limited effect on the volumetric flow rate, resulting in minimal increase in
437 the reaction rate. From an efficiency perspective, the spacing of 25 cm can be the
438 optimal sterilization efficiency spacing for the T-wall system.

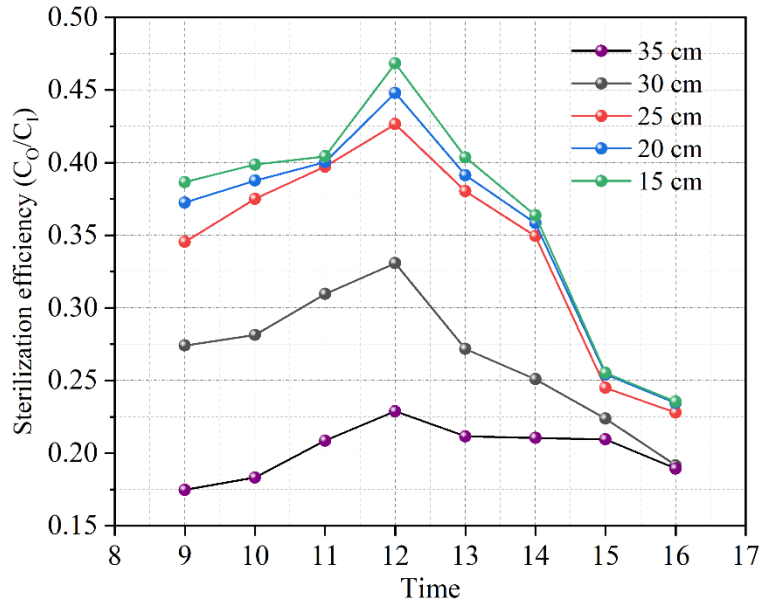


Fig. 11. The sterilization efficiency of the T-wall system under different spacing

Thermal efficiency was used to evaluate the system's ability in converting solar radiation into heat. The thermal efficiency of the system is evaluated by the proportion of thermal energy obtained from the air in the T-wall chamber to the total received solar radiation of the system. The expression is as **Eq. (13)**:

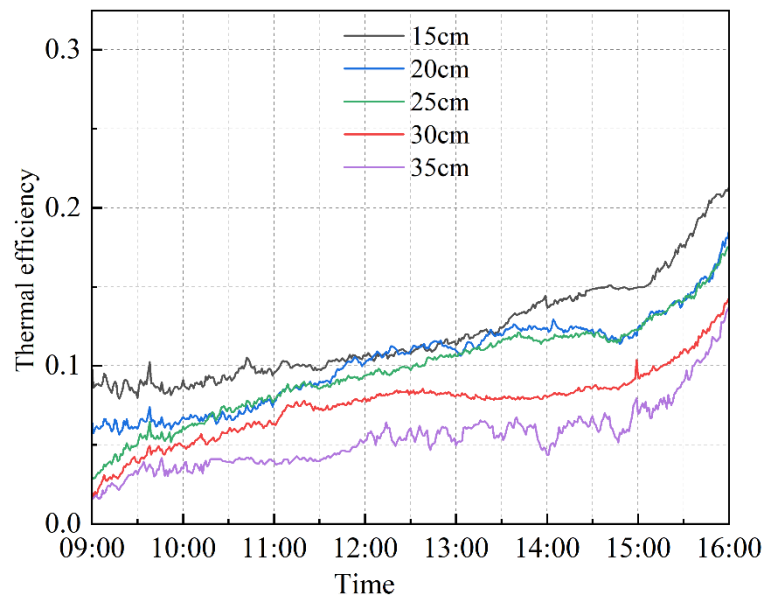
$$\eta_T = \frac{c_{air} V A_{out} (T_{out} - T_{in})}{A_{solar} I_{solar}} \quad (13)$$

Where T_{out} and T_{in} are the air outlet and inlet temperature. A_{out} , m², is the area of the air outlet. A_{solar} , m², is the received area of solar radiation. I_{solar} , W/ m², is the solar radiation intensity.

Fig. 12 shows the thermal efficiency of the T-wall system under different spacing. The thermal efficiency was increased with time. Due to the hysteresis of heat transfer, The curve between thermal efficiency and solar radiation is not similar. Even when solar radiation decreases, the T-wall system continues to heat the air, leading to a sustained thermal efficiency. When the spacing is reduced from 35cm to 15cm, the thermal efficiency of the T-wall system increases. The thermal efficiency values observed are 0.05, 0.075, 0.098, 0.103, and 0.121, respectively. This trend is similar to the trend observed for sterilization efficiency, indicating that reducing the spacing will improve thermal efficiency. When the spacing is reduced to 25cm, further reducing has a limited

459 effect on improving the thermal efficiency.

460



461

462 **Fig. 12.** The thermal efficiency of the T-wall system under different spacing

463 Due to the obstruction of the baffle, solar radiation cannot directly heat the air inside
464 the system cavity. The temperature rise of the air in the T-wall system chamber is mainly
465 achieved through convective and radiative heat transfer through baffles. Reducing the
466 spacing increases the volume flow rate, which enhances convective heat transfer with
467 the baffle. Additionally, according to **Eq. (13)**, increasing the flow rate improves
468 thermal efficiency. Limited by volume flow rate, the optimal spacing for thermal
469 efficiency spacing in the T-wall system is found to be 25 cm, similar to the optimal
470 spacing for sterilization efficiency.

471 Based on the analysis of heating, electricity generation, and sterilization efficiency, the
472 optimal spacing for the T-wall system is determined to be 25 cm. This spacing allows
473 for effective sterilization, efficient heating, and maximum electricity generation.

474

475 **4.3 Optimization of layout of UV light strips for sterilization**
476 **efficiency**

477 UV radiation a widely employed method for control bioaerosol due to its germicidal
478 effect. UV radiation also serves as the driving force for photocatalytic oxidation,
479 making it an effective method for indoor sterilization and disinfection. In this study, we
480 have arranged UV light strips inside the T-wall system chamber as shown in **Fig. 13**.
481 The total length of the light strip is 0.6 m, which is the same as the T-wall system. The
482 UV light strips used in this study are consisted of one light bead every 10cm. Each light
483 bead can give $600 \mu\text{W}/\text{cm}^2$ radiation intensity. The lights emitted short-wave UV
484 radiation with a radiation peak at 253.7 nm for germicidal action. The ultraviolet light
485 strip in the T-wall system is powered by the PV panels, with three PV panels being
486 used to provide the necessary energy.



487
488 **Fig. 13.** The photograph of UV light strips

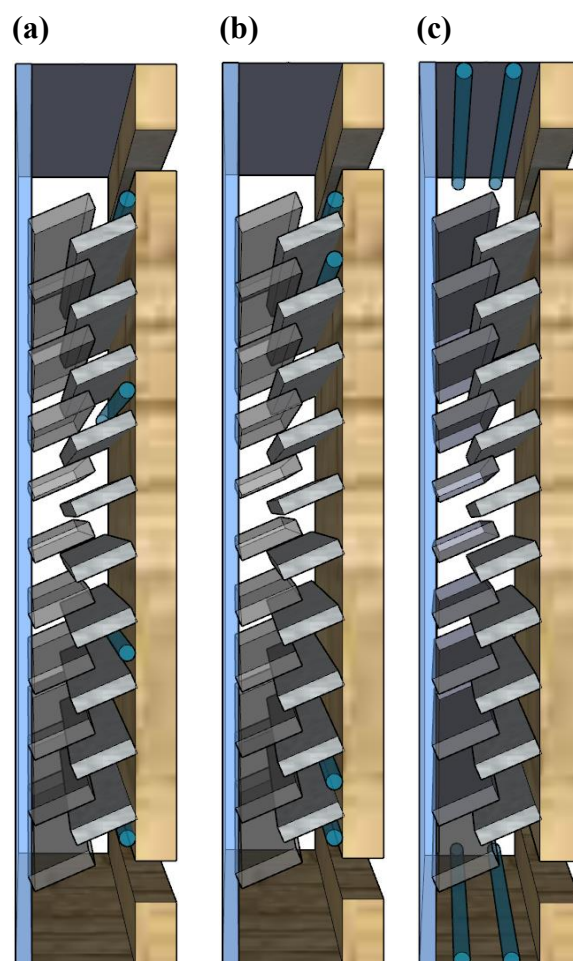
489 The system is equipped with a total of four UV light strips. The layout of UV light
490 would have an impact on sterilization efficiency by affecting the UV dose. UV dose
491 was calculated with the following equations:

492
$$UV \text{ dose } (mJ/cm^2) = \text{radiation intensity } (\mu W/cm^2) \times \text{radiation time } (s)$$

493 Specific UV dose depends on the residence time of the bacterial bioaerosols in the zone.

494 **Fig. 14** shows the different layouts of UV light strips. In this study, three layouts were
495 used: (a) balanced arrangement (b) inlet and outlet arrangement (c) up and down

496 arrangement. The balanced arrangement is designed to arrange the UV light strips at
497 the same spacing on the surface of the thick walls. The inlet and outlet arrangement is
498 designed to concentrate two UV light strips at the air inlet and two UV light strips at
499 the air outlet.. Up and down arrangement is designed to install two UV light strips at
500 the top and two UV light strips at the bottom of the T-wall system.

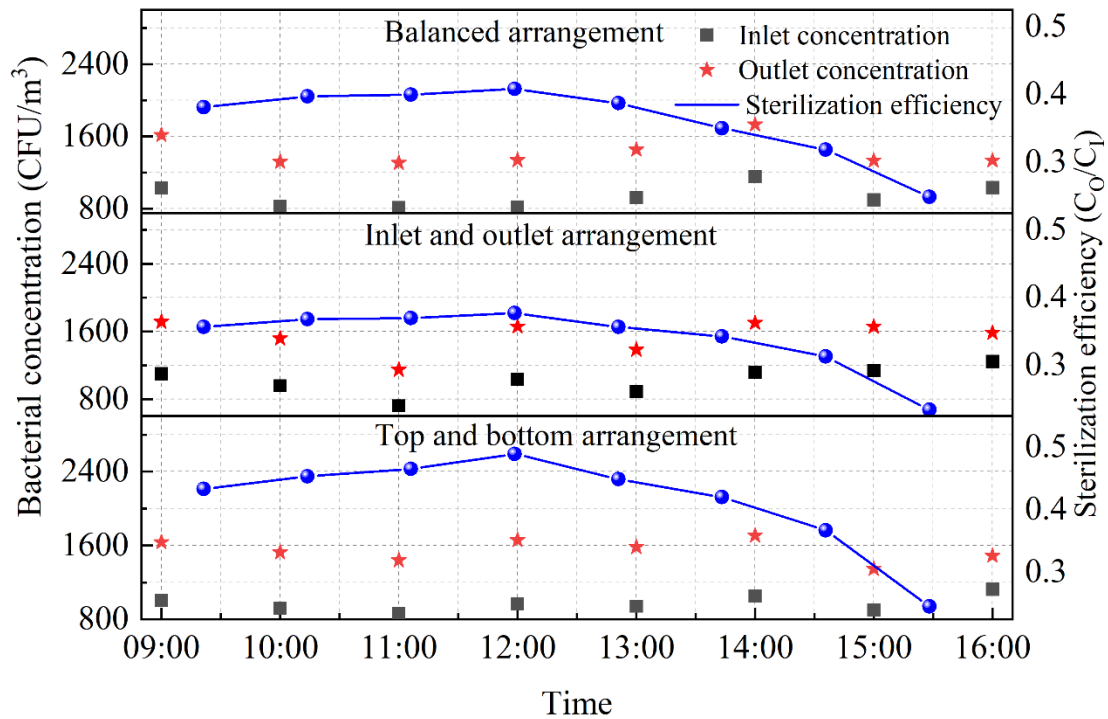


501 **Fig. 14.** The different layouts of UV light strips. (a) balanced arrangement (b) inlet
502 and outlet arrangement (c) up and down arrangement.

503 As shown in **Fig.15**, the installation of UV light strips significantly improved the
504 sterilization efficiency, approaching levels of approximately 20–50% regardless of the
505 layout. Similar to the solar radiation intensity, the sterilization efficiency of the system
506 curve also presents the parabola-type trend. The sterilization efficiency increases with
507 the increasing of solar radiation. This can be attributed to two factors. Firstly, solar
508 radiation affects the sterilization of bacterial aerosols through photocatalytic and

509 thermal catalytic oxidation. Secondly, solar radiation also powers the UV light strips,
510 increasing their radiation intensity as solar radiation intensity rises. Then sterilization
511 efficiency reaches its peak at noon when solar radiation intensity is highest.
512 Subsequently, as the decrease in solar radiation intensity, the sterilization efficiency
513 gradually decreases.

514 As to the layout of UV light strips, it can be seen from **Fig.15**, the top and bottom
515 arrangement has better sterilization efficiency. Sterilization efficiency was in the range
516 of 0.24-0.49 for the whole day and approached 0.49 at noon. The installation of UV
517 light strips at the top and bottom of the system effectively inactivates many bacterial
518 aerosols through irradiation. In addition, the UV light strips located at the top of the
519 system emit radiation onto the photocatalytic membrane, enabling photocatalytic
520 oxidation to take place. Both the radiation intensity of the UV light strips and the
521 catalytic oxidation are significantly influenced by solar radiation. When solar radiation
522 is reduced, a significant decrease in sterilization efficiency can be observed. However,
523 the top and bottom arrangement experiences a faster decrease in sterilization efficiency
524 compared to the other two arrangements as solar radiation decreases. This may due to
525 the open space at the top and bottom of the T-wall system, bacterial aerosols carried by
526 the airflow have a tendency to accumulate in these areas. As for the balanced
527 arrangement and inlet and outlet arrangement of UV light strips, they are designed to
528 irradiate the airflow path, which significantly improve the sterilization efficiency when
529 compared to the syetem without UV light strips. The sterilization efficiency of the
530 balanced arrangement and inlet and outlet arrangement presents a similar variation
531 trend with the top and bottom arrangement. The sterilization efficiency of the balanced
532 arrangement and inlet and outlet arrangement were in the range of 0.249-0.408 and
533 0.234-0.377, respectively. Due to the presence of the baffle, the radiation area for UV
534 light strips in both the balanced arrangement and inlet and outlet arrangement is limited,
535 and the air flow has less exposure time to the radiation. As a result, sterilization
536 efficiency of these arrangement is lower compared to the top and bottom arrangement.



537

538

Fig. 15. The sterilization efficiency of different layouts of UV light strips

539

5. Conclusion

540

A novel Trombe wall was proposed to simultaneously address heating, electricity, and indoor air quality improvement. The performance of heating and electricity generation performance, optimal spacing of the T-wall system, and the impact of different concentrations and layout of UV light strips on sterilization efficiency of were investigated. The main conclusions are summarized as follows:

545

(1) The optimized T-wall system demonstrated a power generation range of 0.06 kWh to 0.298 kWh power and heat output ranging from 6.25 kJ/mol to 17.74 kJ/mol, making it suitable for winter conditions in severe cold regions. The system achieves a sterilization efficiency of 0.204-0.347, making it highly promising for solar-powered indoor air purification applications.

550

(2) The spacing between the baffles in the T-wall system has a significant impact on airflow, heating, electricity generation, and sterilization efficiency. The optimal spacing for the system is found to be 25 cm, as it meets the sterilization efficiency

551

552

553 and heating and balances electricity generation.
554 (3) The sterilization efficiency of the system was further enhanced by the arrangement
555 of UV light strips in the T-wall system. The layout of the top and bottom
556 arrangement facilitates catalytic reactions, resulting in higher sterilization efficiency.

557

558

559 **Authors' contributions**

560 Xiaojian Duan: Writing, Investigation, Data analysis.

561 Chao Shen: Supervision, Writing, Investigation, Resources.

562 Yuoeng Wu: Supervision.

563 **Declaration of conflicting interests**

564 The author(s) declare no potential conflicts of interest with respect to the research,
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