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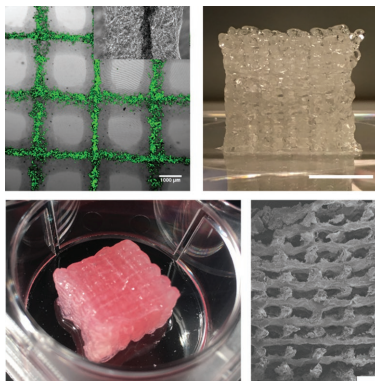
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Communication

Bioprinting Using Mechanically Robust Core-Shell Cell-Laden Hydrogel Strands

P. Mistry, A. Aied, M. Alexander, K. Shakesheff, A. Bennett, J. Yang*

Macromol. Biosci. **2017**, *17*, 1600472



Combining good biological and mechanical properties in bioprinted constructs is desirable for them to be employed in many tissue engineering and regenerative medicine applications. Bioprinted cell-laden constructs with core-shell strands have been developed. The cell-supporting materials in the core support high cell viability and tissue-like functions while the shell material offers mechanical robustness to the bioprinted constructs.

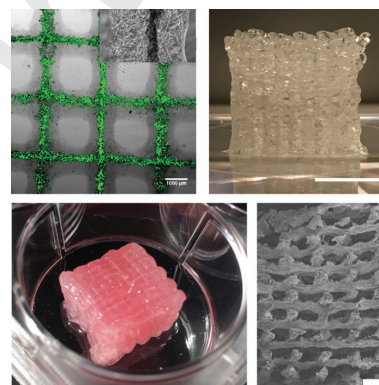
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Bioprinting Using Mechanically Robust Core–Shell Cell-Laden Hydrogel Strands

Pritesh Mistry, Ahmed Aied, Morgan Alexander, Kevin Shakesheff, Andrew Bennett, Jing Yang*

The strand material in extrusion-based bioprinting determines the microenvironments of the embedded cells and the initial mechanical properties of the constructs. One unmet challenge is the combination of optimal biological and mechanical properties in bioprinted constructs. Here, a novel bioprinting method that utilizes core–shell cell-laden strands with a mechanically robust shell and an extracellular matrix-like core has been developed. Cells encapsulated in the strands demonstrate high cell viability and tissue-like functions during cultivation. This process of bioprinting using core–shell strands with optimal biochemical and biomechanical properties represents a new strategy for fabricating functional human tissues and organs.



1. Introduction

The development of highly organized and functional 3D tissue constructs remains an unmet challenge. Bioprinting is emerging as a promising technology for recapitulating 3D hierarchical tissue/organ structures comprising multiple cell types and extracellular matrix (ECM). For bioprinted constructs to survive and function during *in vitro*

maturation, particularly where mechanical stimulation is applied, and after implantation, both the biological and mechanical properties of bioprinted tissue constructs are critical. Hydrogels that are widely used to encapsulate cells in bioprinting, therefore, are required to offer tailored biological and mechanical properties to support the survival and functions of encapsulated cells and maintain the initial structural integrity of the 3D constructs. Despite significant advances in bioprinting of tissues and organs, the combination of optimal biological and mechanical properties in bioprinted cell-laden hydrogel constructs has not been achieved. In this paper, we describe a novel extrusion-based bioprinting process that utilizes core–shell cell-laden strands with a mechanically robust hybrid hydrogel shell and an ECM-mimicking hydrogel core. The ECM-mimicking hydrogels, such as collagen and Matrigel, supported high cell viability and *in vivo* like cell functions, meanwhile the hybrid hydrogel shell supplied mechanical robustness, such as shape recovery after compression. Three different cell types were encapsulated in bioprinted structures consisting of core–shell strands, all of which displayed high cell viability during culture. A vascular-like morphology from the human umbilical vein endothelial cells (HUVECs) and albumin secretion by HepG2 cells in the core were demonstrated. The release rates of two proteins from the strands were found to

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1 correlate with the rate of swelling. These core–shell strands
2 can be used to fabricate hierarchical tissue constructs with
3 desirable biological and mechanical properties.

4 Since the early work in which a microfluidic device was
5 used to make continuous solid and hollow fibers,^[1] a body
6 of work has been published on cell-laden hydrogel fibers/
7 strands with different configurations (solid, hollow, and
8 core–shell configurations) formed by using microfluidic
9 devices^[1–7] as well as extrusion through coaxial
10 needles.^[8–12] To form 3D structures, bioprinting utilizing
11 coaxial needles has been used to fabricate structures with
12 solid,^[7,13] hollow strands,^[10,11] and core–shell strands.^[14,15]
13 However, the materials used in the coaxial bioprinting
14 have not been optimized for optimal cell viability/function
15 and mechanical robustness of the printed constructs.
16 Alginate has been used in these bioprinting processes
17 due to its rapid gelation when encountering multivalent
18 cations. However, alginate lacks cell-binding sites for sup-
19 porting cell spreading,^[16] which resulted in suboptimal
20 cell viability and function in these bioprinted constructs
21 with cell-laden solid or hollow strands. To create an ECM-
22 like microenvironment for encapsulated cells, core–shell
23 fibers with an ECM protein core and an alginate shell
24 have been shown to support the long-term culture of
25 encapsulated cells; these cells exhibited tissue-like mor-
26 phologies and functions.^[6] A purpose-built microfluidic
27 weaving machine was used to assemble these core–shell
28 fibers into higher-order structures.^[6] However, the ability
29 to fabricate complex 3D geometries using the textile
30 manufacturing technology is limited. Moreover, alginate
31 hydrogels are relatively brittle and lack flexibility for in
32 vitro manipulation and implantation. The strategy of
33 combining hydrogels has been found to markedly improve
34 the mechanical properties.^[17–19] However, those hydrogels
35 were made using harsh conditions which inhibited the
36 encapsulation of cells. Recently, a hybrid hydrogel pre-
37 pared under cell-compatible conditions has been used to
38 encapsulate cells, and subsequently it has been 3D printed
39 into various cellular 3D geometries.^[18] While improved
40 toughness and the ability to recover its shape after com-
41 pression were achieved, the hybrid hydrogel lacked the
42 biological properties for optimal cell survival and func-
43 tion. Despite these significant advances in bioprinting
44 using cell-laden strands, one remaining challenge is the
45 bioprinting of tissue-relevant architectures using strands
46 with combined optimal biological and mechanical prop-
47 erties. Here we have developed a novel bioprinting method
48 that utilizes core–shell cell-laden strands, which have a
49 mechanically robust shell and an ECM-like core to achieve
50 both optimal biological and mechanical properties.

51 In our approach, the core–shell strands were bioprinted
52 using a coaxial needle mounted onto a commercial 3D
53 printer (Figure 1A,B). Bioprinting using a coaxial needle
54 was chosen because the core and the shell materials

1 formed a composite strand which combined the
2 cell-supporting and the mechanical properties of the core
3 and the shell, respectively. The central nozzle was per-
4 fused with a cell-laden hydrogel, while the outer nozzle
5 was perfused with a partially crosslinked alginate or a
6 hybrid hydrogel comprising alginate and poly(ethylene
7 glycol) diacrylate (PEGDA). The partial crosslinking gave
8 alginate and the hybrid gel solutions a suitable viscosity
9 range (Figure 1C) for the formation of a continuous strand
10 during the extrusion-based bioprinting process (Movie S1,
11 Supporting Information). 17×10^{-3} M calcium chloride was
12 found to generate a viscosity range that is suitable for
13 the printing of both alginate and hybrid gels. Addition of
14 PEGDA to alginate resulted in an increase in viscosity. How-
15 ever, both the partially crosslinked alginate and hybrid gels
16 showed similar viscosities (Figure 1C), which suggests that
17 the viscosity of the printable gels was mainly determined
18 by the crosslinking caused by calcium ions. The partial
19 crosslinking of the alginate shell eliminated the need to
20 use highly concentrated alginate^[10] to achieve a suitable
21 viscosity for printing, as well as the requirement to co-
22 perfuse highly concentrated calcium chloride in the core to
23 form alginate strands.^[7,11,13] The core–shell configuration
24 also allowed for the inclusion of cell-laden collagen and
25 Matrigel, which are usually too fluidic for shape fixation
26 via the extrusion-based bioprinting method. The core–shell
27 configuration of the printed strands was well defined with
28 the cellular core positioning approximately in the center
29 of the strands (Figure 1D). Cell-laden strands were printed
30 into thick multilayered constructs that would not be pos-
31 sible to fabricate using textile manufacturing methods
32 (Figure 1E,F). We noticed that the partially crosslinked
33 hydrogels were relatively soft, which consequently compro-
34 mised the interconnectivity of pores during printing. This
35 was due to the sinking of strands that were printed above a
36 layer where the gaps between the two supporting strands
37 were wide. Therefore, a coprinting method was devel-
38 oped in which gelatine strands were printed in the gaps
39 between the core–shell strands for supporting, and sub-
40 sequently removed by incubating in cell culture medium
41 at 37 °C (Movie S2, Supporting Information). A 20-layered
42 construct was made using this method (Figure 1E). By
43 immersing the coprinted constructs in a calcium chloride
44 solution and subsequently in culture medium at 37 °C,
45 gelatine was removed efficiently and the shape was main-
46 tained (Figure 1F). Imaging the cross section (side view of
47 the constructs) using scanning electron microscopy (SEM)
48 after the removal of gelatine showed that the pores were
49 open and interconnected (Figure 1G).

50 When a hybrid gel (PEGDA/alginate) was used as the
51 shell material, each layer of a multilayer construct was
52 crosslinked using UV before the next layer was printed on
53 top in order to ensure the uniform crosslinking of PEGDA.
54 Repeated UV exposure during the printing of thick



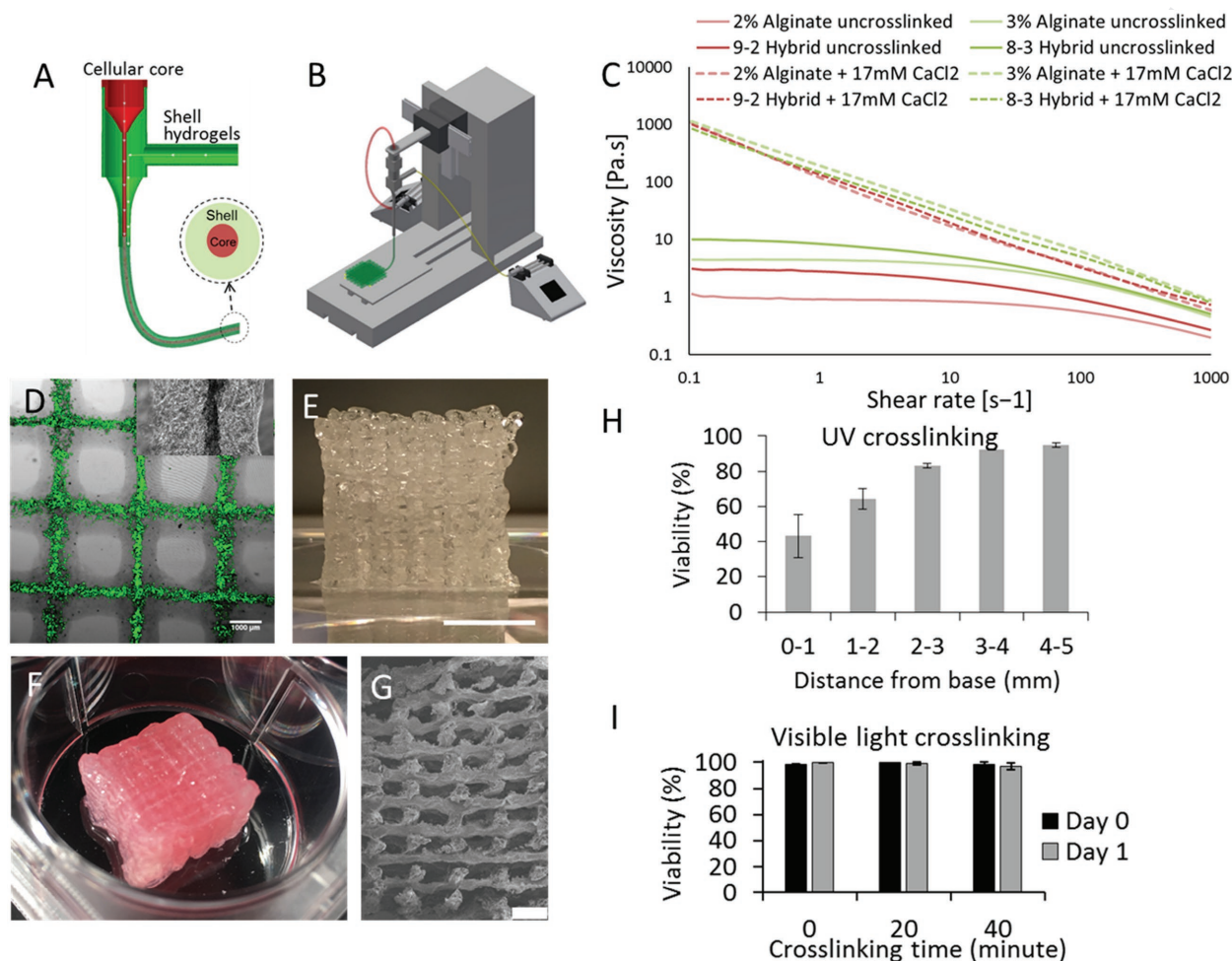


Figure 1. 3D bioprinting using core–shell cell-laden strands. A,B) Schematic diagram depicting the coaxial needle and the printer assembly. C) Viscosities of uncrosslinked and partially crosslinked alginate and hybrid gels. D) A 3D printed lattice comprised of core–shell (hybrid gel) strands with fluorescently labelled cells in the core surrounded by the shell (darker gray). The inset is a bright-field image showing the core and shell. Scale bar: 1 mm. E) A bioprinted 20-layer construct using coprinting of cell-laden core–shell (hybrid gel) strands and gelatine strands. Scale bar: 10 mm. F) A printed construct after removal of gelatine showing structural integrity. G) SEM image of the cross section (side profile) of a bioprinted construct showing interconnected pores after the removal of gelatine. Scale bar: 1 mm. H) Viability of 3T3 fibroblasts in a six-layer construct with 1 min UV exposure for each layer. The construct was manually cut into five layers from base to top for viability evaluation. I) Viability of 3T3 fibroblasts after exposure to visible light for different time periods. Error bars represent standard deviation, $n = 3$.

constructs was found to lower cell viability, which was caused by the penetration of UV light into lower layers during crosslinking of the top layer (Figure 1H). We therefore replaced the UV-activated photoinitiator (Irgacure 2959) with a visible-light-activated photoinitiator (lithium phenyl-2,4,6-trimethyl-benzoylphosphine (LAP)).^[20,21] Cells encapsulated in the visible-light-crosslinked methacrylated gelatine (GelMA) showed high viability, even after long exposure to the light (Figure 1I). Tall Cell-laden constructs could therefore be printed without compromising the viability of cells (Movie S3, Supporting Information). Although the strand diameter (ca. 800 μm) was greater than those made using microfluidic devices (ca. 200 μm), high cell viability was maintained during

culturing (Figure 2), suggesting that transportation of nutrients and oxygen was sufficient through the shell to the cellular core.

To investigate cell survival, morphology, and function within the bioprinted structures constructed from core–shell strands, three different cell types were separately encapsulated in three different core materials. The combinations of cell type and core hydrogel (gelatine methacrylate, collagen, Matrigel) is shown in Figure 2A. High cell viability were maintained during the culture period of 28 d. 3T3 fibroblast culture was terminated at day 7 due to the rapid proliferation and consequent confluence of cells. The cell viabilities between constructs with alginate or the hybrid gel (9:2, PEGDA: alginate

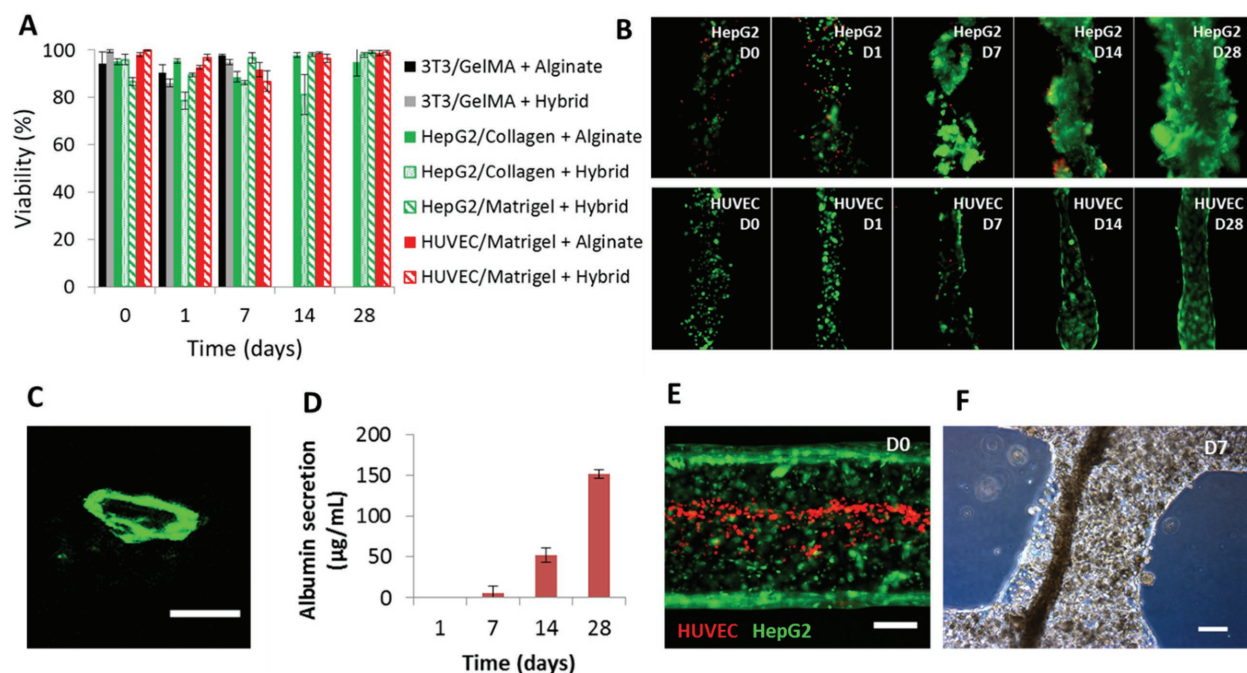


Figure 2. Cell viability, morphology, and function within bioprinted constructs with core-shell strands. A) Viability of three different cell types in the core-shell strands with different core and shell materials. B) Cell morphologies in the cores of core-shell strands during 28 d of culturing. Cells were labelled using green-fluorescent calcein-AM (live cells) and red-fluorescent ethidium homodimer-1 (dead cells). C) Formation of a vascular-like structure from bioprinted HUVECs in a transversely cut core-shell strand at day 44. Scale bar = 100 µm. D) Albumin secretion of HepG2 cells in bioprinted constructs. E, F) Bioprinted HUVECs and HepG2 cells in the core and shell respectively at day 0 and day 7. The cells were fluorescently labelled at day 0 using a red and a green cell tracker, respectively. Scale bar: 200 µm. Error bars represent standard deviation, $n = 3$.

(%) shell were similar. Immediately after printing, the HUVECs appeared discrete and rounded, and were a mixture of individual cells and cell aggregates. The HUVECs began to spread in the Matrigel core by day 1, and had organized themselves to form a vascular-like structure by day 7. This vascular-like structure was maintained from day 7 to day 28. HUVECs were cultured up to 44 d, and showed high cell viability (Figure S1, Supporting Information). On day 44 of the HUVEC culture, the strands were cut transversely to image the cross sections. The formation of a vascular-like structure within the strands was observed (Figure 2C). It appeared that the vascular-like channels were formed at the boundary between the core and the shell (Figure S1, Supporting Information), suggesting that it is possible to control the diameter of the channel by varying the size of the central needle. The embedded HepG2 cells exhibited an increase in albumin secretion over time (Figure 2D), which correlated with the increase in cell numbers as evidenced in Figure 2B.

We have also demonstrated that two different cell types can be coprinted into the core and shell, respectively. Figure 2E shows the bioprinted strands with hepatocytes in the alginate shell and HUVECs in the Matrigel core. After 7 d of cultivation, the HUVECs in the core formed a vascular-like structure, similar to that formed in the strands with an acellular shell (Figure 2F). HepG2

cells in the alginate shell formed multiple cell aggregates. Although the channels formed by the HUVECs are larger than liver sinusoids, this bioprinted multicellular structure is representative of the natural arrangement of endothelial cells and hepatocytes in liver. The capability of including two cell types in the core and shell, respectively, suggests the possibility of fabricating vascularized mini-tissues using these core-shell strands. The cell type in the shell can potentially be changed, implying that these core-shell strands can be used to fabricate different vascularized mini tissues.

Next, we measured the tensile properties of alginate/PEGDA hybrid gels with different compositions. Three hybrid gel compositions (namely 10:1, 9:2, and 8:3, PEGDA:alginate (%)) were examined while the overall hybrid gel concentration was fixed at 11% (w/v). The tensile properties of these materials were assessed using molded dumbbell-shaped samples, and are shown in Figure 3A. Representative stress-strain curves are shown in Figure S2 in the Supporting Information. The modulus and ultimate tensile strength (UTS) of the hybrid gels increased with the concentration of alginate. The strengths of the hybrids were much higher than the sums of the individual components, suggesting a synergistic effect (Figure S3, Supporting Information). This synergistic effect is likely due to the entanglement of alginate

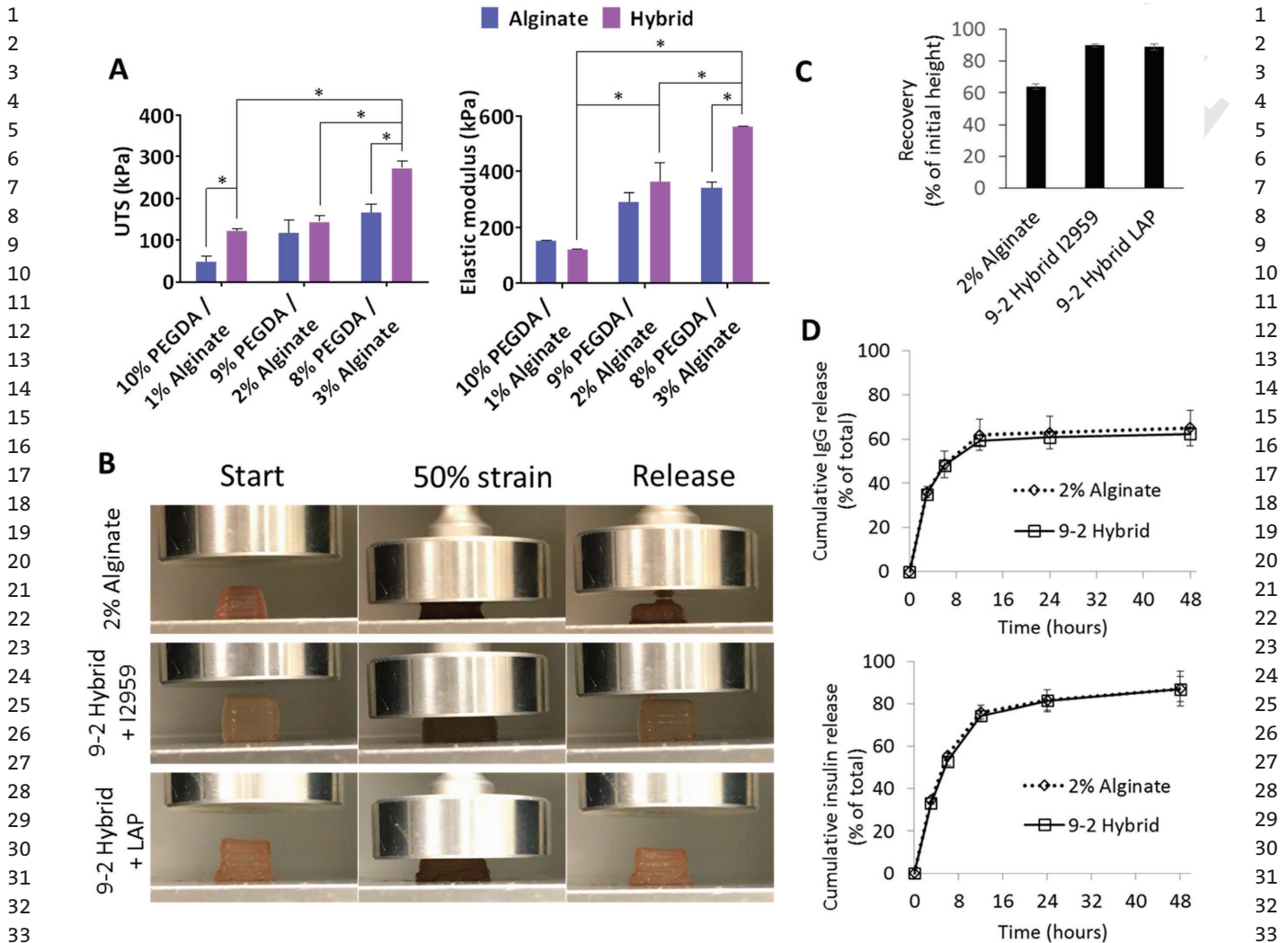


Figure 3. Mechanical properties and protein release properties of bioprinted constructs. A) Tensile properties of dumbbell-shaped hydrogels. B) Shape changes of bioprinted ten-layered solid constructs with cell-laden core–shell strands after compression to 50% strain. C) Quantified shape recovery using the percentage of initial height after compression. D) Human IgG and human insulin release profiles from printed constructs with core–shell strands. Error bars represent standard deviation, $n = 3$. The * sign denotes statistical difference using $\alpha = 0.05$.

and PEGDA chains; chain entanglement in hydrogels is a contributor to their mechanical properties.^[22] The 9:2 and 8:3 hybrid gels showed an increase in all three mechanical properties (modulus, UTS, and failure strain) compared to pure alginate gels, with a maximum 65% increase in UTS for the 8:3 hybrid gels (Table S1, Supporting Information). Up to 3% alginate was used in our study. While higher concentrations can further increase the modulus and strength of gels, they can also reduce the transportation of nutrients^[23–25] and cell viability.^[26,27] Both PEGDA and alginate have been tested in clinical trials and have shown good biocompatibility.^[28,29] In this study, we have used calcium chloride to replace the low-solubility calcium sulfate used in previous studies,^[18] eliminating the presence of solid calcium sulfate particles in the final printed constructs. Though calcium sulfate was shown to be biocompatible

as a bone substitute in animal testing,^[30] its presence may not be desirable in other applications. Bioprinted solid constructs with cell-laden core–shell strands were assessed using compression testing. The constructs were compressed to 50% of their original height and then released immediately. The printed constructs with the hybrid gel (9:2, PEGDA:alginate (%)) showed significantly more shape recovery compared to pure alginate counterparts.

The degradation of the core and shell materials used in our study has been previously reported. The core materials (collagen I, Matrigel, GelMA) are likely to degrade faster than the shell materials (PEGDA and alginate) due to enzymatic degradation of these protein-based materials.^[31–33] The degradation of PEGDA has been attributed to the hydrolysis of the esters rather than the backbone ethers.^[34] The modulus of PEGDA, which was implanted

1 in a rat, showed progressive reduction at an average rate
2 of 6% per week. Degradation of alginate relies on the
3 gradual exchange of calcium, which crosslinks guluronic
4 acid blocks, for monovalent cations.^[35] Oxidation can
5 also be used to make alginate degradable under physi-
6 ological conditions.^[36] The difference in degradation rates
7 means that the remodeling processes in the core and the
8 shell, respectively, are different. The shell material would
9 remain longer than the core material after implantation,
10 which is beneficial for maintaining structural stability.

11 These core–shell strands can potentially be used for
12 immunoprotective roles to encapsulate allogenic cells or
13 for delivering therapeutic proteins. To test the release of
14 proteins from the strands, two proteins of different sizes
15 were studied: human insulin (6.6 kDa) and human IgG
16 (150 kDa). Figure 3D shows the release profiles of proteins
17 from the bioprinted constructs with core–shell strands.
18 The results show no significant differences between the
19 hybrid shell and the pure alginate shell, suggesting that
20 the addition of crosslinked PEGDA does not reduce the
21 overall mesh size significantly, with regard to the sizes
22 of the investigated proteins. The cumulative release of
23 insulin is greater than that of IgG, suggesting that higher-
24 molecular-weight proteins are more likely to be entrapped
25 within the gels. The times at which the protein releases
26 started to plateau were similar to the time (11 h) at which
27 the swelling reached maximum (Figure S4, Supporting
28 Information), suggesting the rapid release may be related
29 to the increase of hydrogel mesh size caused by swelling.
30 The rate of protein release agrees with previous observa-
31 tions made on protein release from alginate beads.^[37,38]

32 In summary, we have bioprinted 3D structures with
33 core–shell strands that have a mechanically robust shell
34 and an ECM-mimicking core. Interconnected pores were
35 introduced by using a coprinting process. Bioprinting
36 using the core–shell hydrogel strands allows more com-
37 plex 3D geometries to be formed compared to textile
38 manufacturing methods. Compared to previous coaxial
39 bioprinting, the materials we employed enhanced the
40 mechanical robustness of the constructs, and the survival
41 and function of encapsulated cells. Separately encapsu-
42 lated, three cell types in the core showed high viability
43 within bioprinted constructs consisting of core–shell
44 strands. The formation of a tissue-like morphology by
45 the HUVECs was also observed. In addition, we were able
46 to coprint endothelial cells in the core and HepG2 cells
47 in the shell to fabricate mini tissues with vascular-like
48 structures, which can potentially be assembled to form
49 larger and more complex tissues using bioprinting. By
50 adding PEGDA to alginate, the hybrid gels showed greater
51 tensile moduli and strengths compared to pure alginate.
52 The shape recovery after compression was also signifi-
53 cantly improved by using hybrid gel strands. The rates
54 of protein diffusion through the alginate and hybrid gel

1 shell showed no difference. This process of bioprinting
2 using core–shell strands with combined biochemical and
3 biomechanical properties represents a new strategy for
4 fabricating functional human tissues and organs.

2. Experimental Section

2.1. 3D Bioprinting with Core–Shell Strands

10 Constructs with core–shell strands were printed using a
11 coaxial needle (27G/18G inner and outer needles, respectively)
12 mounted onto a commercial 3D bioprinter (RegenHU, Switzer-
13 land). The core and shell were driven by two separate syringe
14 pumps using flow rates of 0.01 and 0.1 mL min⁻¹, respec-
15 tively. Hydrogel solutions for the shell were prepared by dis-
16 solving either PEGDA (20 kDa; Sigma-Aldrich) or alginate (FMC
17 Biopolymer) individually, or in combination, in deionized water
18 at the desired (w/v) concentrations. For the hybrid hydrogels,
19 the total hydrogel concentration was fixed at 11% (w/v). Irga-
20 cure 2959 (I2959; Sigma-Aldrich) or LAP (TCI Chemicals) was
21 added as the photoinitiator at a final concentration of 0.1% or
22 0.13% (w/v), respectively, in the hybrid gel solutions. The shell
23 hydrogel solutions were partially crosslinked by mixing with
24 calcium chloride solutions to reach a final concentration of
25 17 × 10⁻³ M calcium ions. For strands with the LAP photoinitiator,
26 visible light (Schott KL1500 LCD) was shone continuously during
27 printing; for strands with the I2959 photoinitiator, UV (power:
28 15 W; λ: 365 nm; working distance: 35 mm; UVP Cambridge,
29 UK) was shone for 1 min per layer during printing. These con-
30 structs were then immersed in a calcium containing buffer
31 (100 × 10⁻³ M CaCl₂, 150 × 10⁻³ M NaCl, 25 × 10⁻³ M HEPES, phenol
32 red indicator, deionized water, pH 7.5) for 10 min. The core
33 materials of collagen (Corning) and Matrigel (BD Bioscience)
34 were printed at 5 °C to prevent crosslinking in the cartridge.
35 Type I rat tail tendon collagen was used at a concentration of
36 3 mg mL⁻¹. GelMA was prepared as described previously,^[39]
37 and 5% (w/v) GelMA in culture medium was used. Four mil-
38 lion cells per milliliter were used as the cell density in all cores.
39 6% (w/v) gelatine was used in the coprinting process.

2.2. Formation of Dumbbell-Shaped Hydrogel Samples

41 All gels were cast in a dumbbell-shaped PTFE mold. The samples
42 had a thickness of 3 mm and a length of 10 mm for the reduced
43 section. If PEGDA was included, the hydrogel solutions were first
44 cured with UV for 2 min before the crosslinking of alginate in a
45 CaCl₂ solution (100 × 10⁻³ M) for 10 min. Pure alginate hydrogels
46 were prepared by first pre-crosslinking with a CaSO₄ slurry at a
47 fixed alginate:CaSO₄ ratio of 1:0.1328. The solution was immedi-
48 ately cast into the mold and left for 5 min with a glass slide to
49 cover the top. The pure alginate hydrogels were then immersed
50 in a 100 × 10⁻³ M CaCl₂ bath for 10 min.

2.3. Tensile and Compression Testing of Hydrogels

53 The tensile properties the hydrogels were measured at room
54 temperature using a Universal Texture Analyser (TA-HD Plus,

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Stable Microsystems, USA). The grip section of each dumbbell-shaped gel was wrapped with paper towel to improve gripping. A constant deformation speed of 0.5 mm s^{-1} was applied during the test. The tests were stopped after the samples broke. Compression testing was carried out using the same machine on bioprinted solid constructs ($8 \times 8 \times 8 \text{ mm}^3$, ten layers) with cell-laden core–shell strands.

2.4. Cell Culture

All cells were cultured at 37°C with 5% CO_2 . HepG2 cells (ATCC) were used up to passage 20, and were cultured in Eagle's minimal essential medium (Sigma-Aldrich) supplemented with 9% (v/v) fetal bovine serum (FBS; Sigma-Aldrich), $2 \times 10^{-3} \text{ M}$ L-glutamine (Sigma-Aldrich), 1% nonessential amino acids (Gibco), and 1% antibiotic/antimycotic (Sigma-Aldrich). The 3T3 mouse fibroblast (3T3) cell line (ATCC) was used up to passage 65, and were cultured in DMEM supplemented with 9% FBS, $2 \times 10^{-3} \text{ M}$ L-glutamine, and 1% antibiotic/antimycotic. Primary HUVECs (PromoCell) were used up to passage 6, and were cultured in endothelial cell basal medium (PromoCell).

2.5. Cell Viability and Albumin Secretion

Cell viability was measured using a live/dead kit (ThermoFisher, UK). To measure cell viability in LAP crosslinked GelMA, one million cells per milliliter of 3T3 fibroblasts were encapsulated in 5% (w/v) GelMA containing 0.13% (w/v) LAP. Light (working distance: 25 mm) was shone on the gels for different time periods, after which culture media was added.

Fluorescent images were taken using a fluorescence microscope (Leica). The albumin secretion was measured using an ELISA kit (Abcam, UK) and a plate reader (Infinite M200, Tecan).

2.6. Protein Release Studies

Lattice constructs ($20 \times 20 \times 1.6 \text{ mm}^3$, two layers) were printed with a core of GelMA (5%) loaded with either recombinant human insulin (Sigma-Aldrich) or recombinant human IgG (Sigma-Aldrich). The concentrations of insulin and IgG in the cores were 174 and $10 \mu\text{g mL}^{-1}$ respectively. Constructs were incubated in culture medium at 37°C . At regular intervals, the medium was taken and replaced with fresh medium. ELISA was used to examine the medium samples for the presence of insulin (Simple-Step Human Insulin ELISA; Abcam) or IgG by (Human IgG ELISA; Sigma-Aldrich).

2.7. Statistical Analysis

One-way ANOVA with Tukey's posthoc test was used for statistical analysis. An α value of 0.05 was used in both methods.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

Acknowledgements: The authors would like to thank EPSRC and MRC Centre for Doctoral Training in Regenerative Medicine for sponsoring Pritesh Mistry's studentship.

Received: November 9, 2016; Published online: ; DOI: 10.1002/mabi.201600472

Keywords: bioprinting; hydrogels; mechanical properties; tissue engineering

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