

A Review of Predictive Control Techniques for Matrix Converter Applications

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Abstract—Predictive control has recently emerged as a promising alternative to more traditional methods for the control and modulation of power converters. This paper presents an overview of predictive control techniques applied to matrix converters. The paper highlights that predictive control strategy is a promising alternative to conventional modulator based linear control for matrix converters due to its simplicity and flexibility to include additional constraints within the control to have it suitable for different applications. In addition to describing many advantages of predictive control techniques, its limitations and weaknesses are also discussed along with some future trends and applications. Most important control aspects of predictive control are demonstrated through simulation analysis.

Index Terms—ac-ac conversion, matrix converter, predictive control, modulation schemes.

NOMENCLATURE

\mathbf{i}_s	Source currents	$[i_{sA} \ i_{sB} \ i_{sC}]^T$
\mathbf{v}_s	Source voltages	$[v_{sA} \ v_{sB} \ v_{sC}]^T$
\mathbf{i}_i	Input currents	$[i_A \ i_B \ i_C]^T$
\mathbf{v}_i	Input voltages	$[v_A \ v_B \ v_C]^T$
\mathbf{i}_o	Output currents	$[i_a \ i_b \ i_c]^T$
\mathbf{v}_o	Output voltages	$[v_a \ v_b \ v_c]^T$
\mathbf{i}_s^*	Source current references	$[i_{sA}^* \ i_{sB}^* \ i_{sC}^*]^T$
\mathbf{i}_o^*	Output current references	$[i_a^* \ i_b^* \ i_c^*]^T$
\mathbf{v}_o^*	Output voltage references	$[v_a^* \ v_b^* \ v_c^*]^T$
C_f	Input filter capacitor	
L_f	Input filter inductor	
R_f	Input filter resistor	
R_L	Load resistance	
L_L	Load inductance	

I. INTRODUCTION

The matrix converter (MC) shown in Fig. 1 is a simple power conversion circuit that directly connects the *ac*-source with any arbitrary *ac*-load without the need for large storage elements (*dc* capacitors and inductors), making this topology suitable for many applications where weight and size are important issues. With the MC topologies, generation of output voltages of any amplitude and frequency, operation with sinusoidal input and output current waveforms, control with unity displacement power factor, and regenerative capability are all possible. The major challenge with MCs is the commutation of current between the bidirectional switches, however this issue has been solved with multi-step commutation techniques [1], [2]. Due to many favorable characteristics and benefits, in recent years, the MCs have shown continuous and rapid

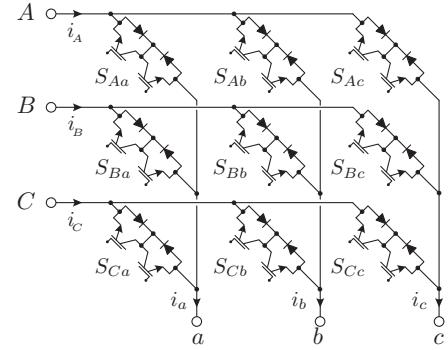


Fig. 1. Power circuit of conventional direct matrix converter.

development in terms of new topologies and control schemes investigation, including industrial applications with standard MC units for high and medium voltage using cascaded connections [3], [4].

Various modulation and control methods have been proposed in the literature for MCs [5]–[38]. These methods have different digital implementations and different levels of complexity, but they all have dynamic performance which is acceptable in a variety of applications. As reviewed in [39] and shown in Fig. 2, the most commonly used techniques are Venturini [5], carrier-based pulse width modulation (PWM) [7], [8], space vector modulation (SVM) [9], [10] and direct torque control (DTC) [11], [12]. Other control methods that have been applied to MCs in specific applications are fuzzy control, neural networks and genetic algorithms [40], [41]. Due to the discrete nature, intuitive approach and simplicity of MCs for real-time implementation, the predictive control has shown to be a very promising alternative to control MCs [15]–[38].

The objective of this paper is to provide an overview of contributions and trends in the application of predictive control techniques for MCs, including variations of the control strategies employed as well as the applications where they have been implemented. The paper highlights that predictive control can be easily implemented by taking advantage of commercially-available digital signal processor platforms/technologies. In addition to the open questions and future trends, the limitations and weaknesses of predictive control in comparison to conventional control techniques are discussed.

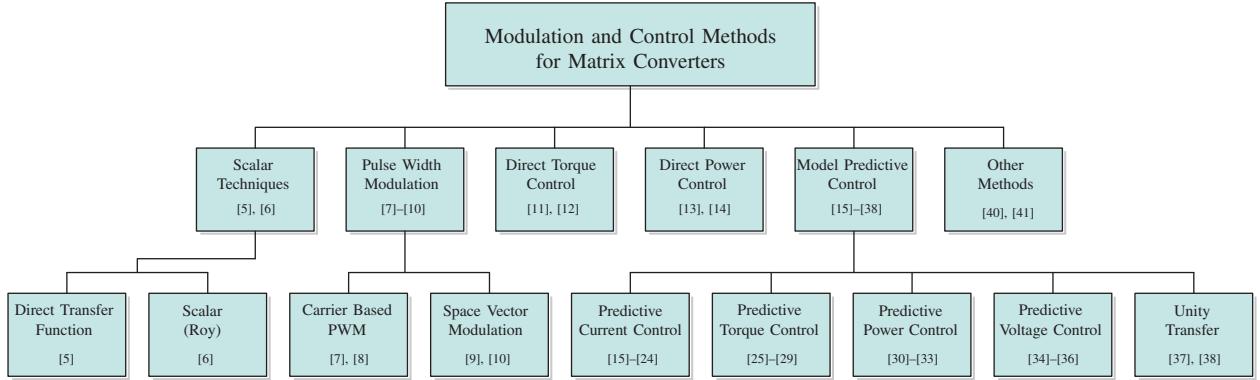


Fig. 2. Summary of modulation and control methods for matrix converters.

II. CONVENTIONAL MODULATION AND CONTROL

The power topology of standard direct MC is presented in Fig. 1. The circuit consists of bidirectional switches that directly connect any input line to any output line at any point in time. A harmonic filter is normally used at the input-side with the following two purposes [1], [2]:

- To provide a low impedance path which avoids the generation of over-voltages due to fast commutation of currents between the bidirectional switches.
- To attenuate high-frequency harmonics in the input currents in order to meet any relevant input power quality standards.

The operation of any MC is restricted by two constraints:

- The load current cannot be interrupted due to the inductive nature of the load.
- The operation of switches should not involve short circuiting of any of the input lines.

These restrictions are expressed by:

$$S_{Ay} + S_{By} + S_{Cy} = 1, \quad \forall \{y = a, b, c\}. \quad (1)$$

The relationship between input and output variables of a MC is given by:

$$\mathbf{v}_o = \mathbf{T}(S_{ij}) \mathbf{v}_i \quad (2)$$

$$\mathbf{i}_i = \mathbf{T}(S_{ij})^T \mathbf{i}_o \quad (3)$$

where $\mathbf{T}(S_{ij})$ is the instantaneous transfer matrix defined by

$$\mathbf{T}(S_{ij}) = \begin{bmatrix} S_{Aa} & S_{Ba} & S_{Ca} \\ S_{Ab} & S_{Bb} & S_{Cb} \\ S_{Ac} & S_{Bc} & S_{Cc} \end{bmatrix}. \quad (4)$$

Equations (2) and (3) form the basis of all MC modulation methods which consist of selecting appropriate combinations of “on” and “off” switches to achieve the desired converter output voltages [1], [2].

III. PRINCIPLES OF PREDICTIVE CONTROL FOR MATRIX CONVERTERS

Finite control-set model predictive control (FCS-MPC), simply called MPC from here onwards, is a digital control

technique which has recently been applied to control the power converters. This control method utilizes a mathematical model of the controlled system in order to predict, at each sampling instant k , the system’s behavior at $k + 1$. In order to select the optimal state of the power converter during each time period, a cost function is defined. This function is composed using several elements or control objectives. Each element can represent specific constraints, such as limitation of switching frequency or other nonlinearities. Constraints contain the difference between the reference and predicted values of the variables to be controlled. As an example, the predictive current control (PCC) for the direct MC (DMC) is presented in this section. The PCC scheme in Fig. 3 shows the switching state selection for a DMC, which displays the nearest references to the controlled variable at the end of each sampling period, respectively. This control approach utilizes the converter and load models in order to predict the future value of currents. A simple and representative model of the load can be expressed as:

$$\frac{d\mathbf{i}_o}{dt} = \frac{1}{L_L} \mathbf{v}_o - \frac{R_L}{L_L} \mathbf{i}_o. \quad (5)$$

Knowing the nature of the load, a first order discrete approximation allows predicting the future load current:

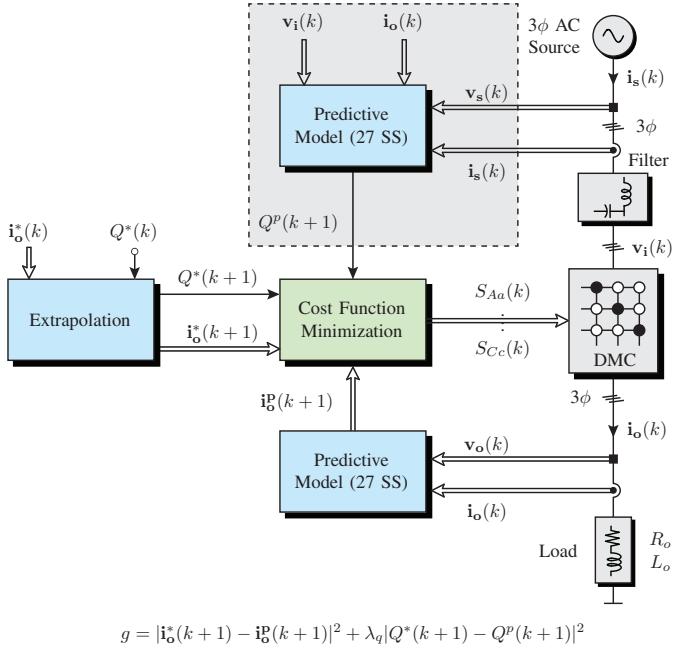
$$\mathbf{i}_o(k+1) \approx \frac{T_s \mathbf{v}_o(k+1) + L_L \mathbf{i}_o(k)}{L_L + R_L T_s} \quad (6)$$

where T_s corresponds to the discretization sampling time.

A cost function is defined in order to determine the error between the reference currents \mathbf{i}_o^* , and their respective predicted currents \mathbf{i}_o^p , given by:

$$g(k) = |i_a^* - i_a^p| + |i_b^* - i_b^p| + |i_c^* - i_c^p| \quad (7)$$

As reported in [15]–[24] this strategy executes well with a very good performance during both steady-state and transient conditions showing to be a very respectable alternative to the classical control schemes. Similar techniques can be applied with cost functions representing other system variables and constraints as well as weighted combinations of system variables. In addition to the DMC there are several topology variations [3], [4].



$$g(k) = |i_o^*(k+1) - i_o^p(k+1)|^2 + \lambda_q |Q^*(k+1) - Q^p(k+1)|^2$$

Fig. 3. Block diagram of PCC with instantaneous input reactive power minimization for DMC.

The main differences between the topologies are in the number/arrangement of the switches, operation constraints and applications. The most important advantages of these topology variations are the increment of output voltage control range and reduction of switching frequency harmonics, losses and common-mode voltage. It is of course possible to apply the principles of MPC to any of the derived MC topologies including indirect MC (IMC) [15], [18], [21], [23], [24]. In [34]–[36], predictive controllers for a single-phase MC application (SPMCs) were proposed. The most popular of these derived MC topologies is the IMC, being implemented using predictive controllers with a variety of cost functions [15], [18], [21], [23], [24], [26], [28], [40]. In this paper, the presented examples will assume a DMC; but all the techniques can be applied to any MC topology.

IV. PREDICTIVE CONTROL STRATEGIES AND APPLICATIONS

Based on previously reported scholarly works, there are several implementations of MPC which have successfully been applied in MC applications. As indicated in Fig. 2, the most relevant techniques correspond to PCC [15]–[24] and predictive torque control (PTC) [25]–[29]. It is also possible to find some implementations of predictive reactive/active power control (PPC) [30]–[33], and predictive voltage control (PVC) [34]–[36] where an *LC* filter is used at the output of MC to provide a voltage source rather than a conventional load control function.

A. Basic Current Control

In this section, different PCC implementations are discussed in regards to specific applications and control objectives. The

basic PCC strategy consists in the load's current control while reducing the instantaneous reactive power at the input side of the converter (Fig. 3). The cost function is now defined as:

$$g(k) = \Delta \mathbf{i}_o + \lambda_q \Delta Q \quad (8)$$

where λ_q is the weighting factor for input reactive power minimization. By including the instantaneous reactive power minimization for the MC input it is possible to obtain unity power factor. However, it has been observed that the PCC, using the reactive power minimization term, is very sensitive to the distortion of the source voltage and resonance of the input filter [16] (before $t=0.06[\text{s}]$). By implementing active damping method (after $t=0.06[\text{s}]$), it is possible to improve the performance of the system by mitigating the resonances of the input filter [16], [17]. It is also possible to force the source current to follow a sinusoidal reference value, regardless of the distortion level at the input side. The cost function for this modified scheme is defined by

$$g(k) = \Delta \mathbf{i}_o + \lambda_i \Delta \mathbf{i}_s \quad (9)$$

where $\Delta \mathbf{i}_s = |i_{sA}^* - i_{sA}^p| + |i_{sB}^* - i_{sB}^p| + |i_{sC}^* - i_{sC}^p|$. The results shown in Fig. 5 and in [15], [17], [23] demonstrate that by imposing a given waveform for the source current, it is possible to obtain a better performance than with an instantaneous reactive power minimization (Fig. 4), reducing the total harmonic distortion (THD) of both input and load currents.

B. Induction Motor Control

A different approach for the control of an induction machine with PCC using instantaneous reactive power minimization is presented in [20]. In this control method, the predictive stage performs PCC, while a classic control stage regulates speed, flux, and torque based on field-oriented control (FOC). The classic control stage provides reference currents for the predictive control stage. With this strategy, predictive control has been demonstrated to be a very powerful tool opening new possibilities in the control of power converters in a simple and intuitive way.

C. Switching Frequency Reduction

Similarly, a PCC for an induction machine with a reduction in converter switching losses is presented in [19], and this approach uses modified cost function in comparison to [20]. In order to reduce the switching frequency and increase the efficiency of converter, the number of commutations n during each sampling instant are minimized as demonstrated below:

$$g(k) = \Delta \mathbf{i}_o + \lambda_q \Delta Q + \lambda_{sw} n \quad (10)$$

With this additional term in the cost function, the switching or changing of state of the converter will have an associated cost, thus reducing the switching frequency at an expense of waveform quality. A further development of this idea in [19] not only reduces the number of commutations, but also the switching losses produced by the switching of power converter.

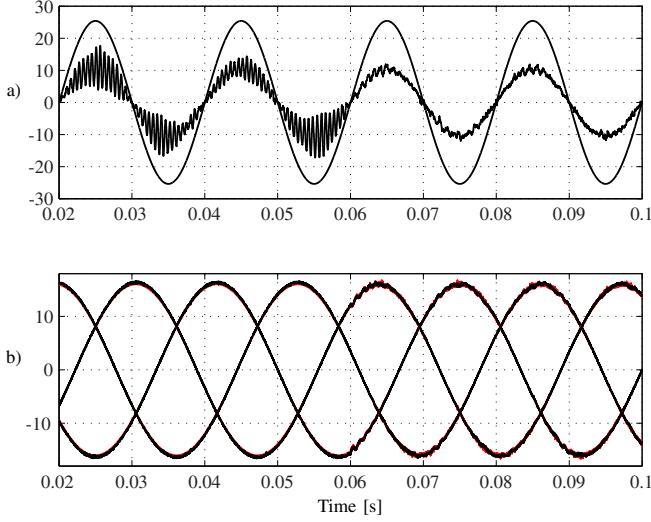


Fig. 4. PCC with instantaneous reactive power minimization, before $t=0.06[\text{s}]$ without active damping implementation, after $t=0.06[\text{s}]$ with active damping implementation: a) source voltage v_{sA} [V] and current i_{sA} [A]; b) output current i_a [A] and its reference i_a^* [A].

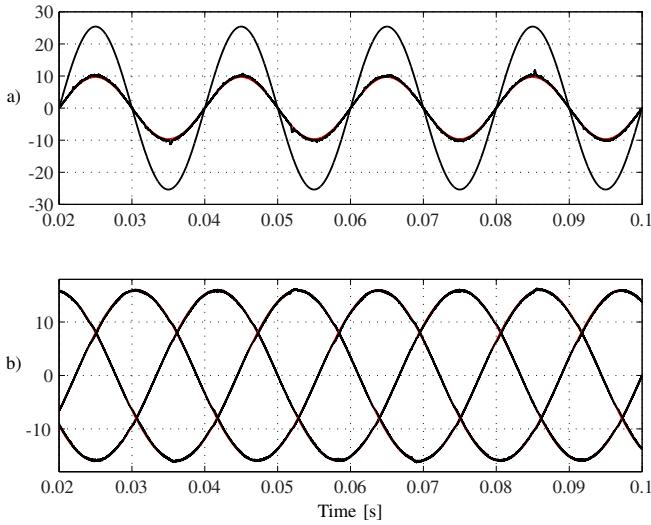


Fig. 5. Predictive current control with imposed sinusoidal source current control: a) source voltage v_{sA} [V] and current i_{sA} [A]; b) output current i_a [A] and its reference i_a^* [A].

D. Common Mode Voltage

In [15], a PCC with imposed source current is proposed with an additional term to reduce common mode voltage (CMV). The resulting cost function is given by:

$$g(k) = \Delta i_o + \lambda_i \Delta i_s + \lambda_v |v_{cm}(k+1)| \quad (11)$$

where the common-mode voltage is defined as $v_{cm} = (v_a + v_b + v_c)/3$. The results showed in [15] demonstrate that with proper definition of cost function, simultaneous control of input and output (source and load) currents is possible along with CMV minimization.

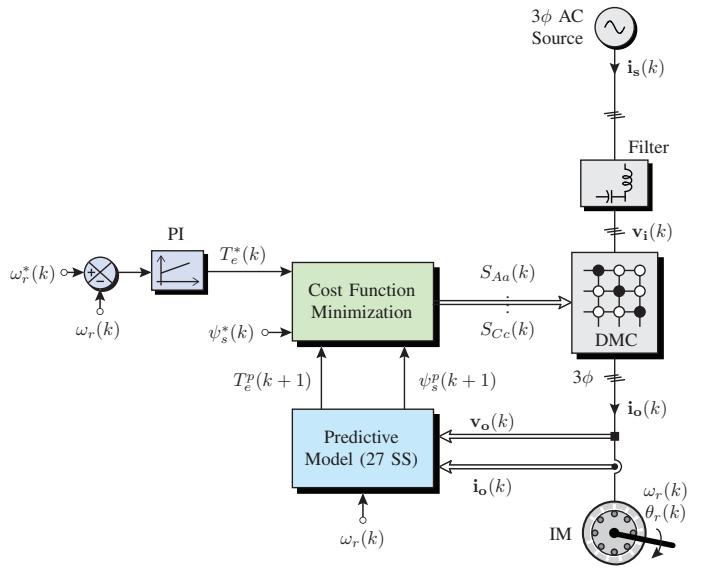
E. Torque Control

Fig. 6 shows the basic control scheme for PTC strategy introduced in [25], [26]. Similar to the PCC method, the PTC consists of selecting, at fixed sampling periods, one of the possible switching states of the matrix converter. Again, selection of the switching state for the next sampling instant is performed by using a predefined cost function minimization. This cost function g represents the evaluation criteria in order to select the best switching state for the next sampling interval. For the computation of the cost function g , the input current i_s , the electromagnetic torque T_e , and the stator flux ψ_s are predicted in the future sampling period, using the mathematical model of the input filter and the induction machine. A PI controller is adopted to generate the reference torque T_e^* . A mathematical discrete-time model is used to predict the behavior of the system under a particular switching state, based on dynamic model for the induction motor [25], [26]. This model is used to predict the stator flux and the electromagnetic torque produced by the machine during the next sampling period.

The cost function is composed of the absolute errors in the predicted torque, flux magnitude and reactive input power, resulting in:

$$g(k) = \Delta T_e(k+1) + \lambda_\psi \Delta \psi(k+1) \quad (12)$$

where λ_ψ is weight factor for stator flux control. It is also possible to add the instantaneous reactive power to the cost function in order to improve the input waveforms [27]–[29]. This method is very simple to implement as well as effective with a high-speed dynamic response of electrical torque and with decoupled control between the torque and stator flux. At the same time, unity displacement power factor for both



$$g = |T_e^*(k) - T_e^p(k+1)| + \lambda_\psi |\psi_s^*(k) - \psi_s^p(k+1)|$$

Fig. 6. Block diagram of PTC scheme for DMC fed induction machine.

motoring and regeneration operation modes is possible. All these remarkable characteristics make PTC a suitable alternative to the direct torque control (DTC) with the advantages of being simpler to implement and considering all the available switching states of the converter. As indicated in Fig. 2 other goals uses for predictive control are also possible in MC applications, including power control [30]–[33] and voltage control [34]–[36]. All these control schemes have been proven in practical implementations and can be analyzed in a similar way to the PCC and PTC in examples discussed earlier.

V. LIMITATIONS, WEAKNESSES AND FUTURE TRENDS IN PREDICTIVE CONTROL FOR MATRIX CONVERTERS

It has been shown that predictive control can be a very powerful alternative to classical modulation and control in MC applications, but this technique also presents some limitations and weaknesses, such as:

- Variable switching frequency.
- High dependence on the model's parameters.
- High sampling frequency and computational cost.

In some applications of predictive control, high sampling frequencies are required to meet any specific power quality requirements [30]. These high sampling frequencies can be met at the higher end of capabilities of currently used control platforms, but the impact of this issue will reduce as microprocessor technology continues to develop. The MC always requires an input filter for correct operation along with having to meet power quality regulations [42]. This filter is usually implemented as an *LC* filter. The spread spectrum nature of predictive control can cause this filter to resonate and either a very high sampling frequency must be used or damping technique must be provided. The first solution results in lower THD in the converter waveforms, but will increase the converter losses and electromagnetic interference (EMI). In [43] an input filter resonance mitigation technique has been proposed to resolve this issue. A damping resistor in the MC input filter will also damp any oscillations, but this resistor will reduce the converter efficiency. An alternative approach is to use active damping, which can improve the input current quality and minimize the instantaneous reactive input power. However, this method only mitigates higher current harmonics resulted from the switching operation and cannot ensure sinusoidal input currents, particularly when the source voltage is distorted [16], [17]. To overcome these issues, in the implementations done with predictive control, the term that minimizes the reactive power at the input side is replaced by a direct control of source currents. This approach forces the input currents to follow the sinusoidal value, regardless of the distortion level at input side [15], [17], [23].

One of the main drawbacks of predictive control methods is that the control can choose only from a limited number of valid switching states in each sampling period. When the sampling frequency is lower than required, it generates noise as well as large voltage and current ripples. The variable switching frequency produces a spread spectrum, decreasing the performance of the system in terms of power quality.

This problem has been recently solved by using predictive control to emulate the implementation of PWM or space vector modulation (SVM) with a linear PI controller [44], [45].

Higher converter switching frequencies can lead to increase issues with EMI emissions from all power converters. Predictive control implementations can lead to high power semiconductor switching frequencies under some operating conditions. It is therefore sometimes necessary to consider including these factors in the cost function to minimize the size and weight of any required EMI filtering associated with the converter application [19], [29].

VI. CONCLUSIONS

This paper presents an overview of different control strategies and applications for matrix converters where predictive control techniques have been applied. It has been demonstrated that predictive control can be recognized as an attractive control approach, with significant benefits such as flexibility, versatility, and performance, with real applications of power converters and electric drives. Nevertheless, there are still some limitations and weaknesses which constitute a future open topic allowing for future research activity on this topic.

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